### Appendix 2-2

### **Grid Connection Package**

### Contents

**Drawing Issue Sheet** 

Site Layout Plans

Underground Cable Section Drawings

Watercourse Crossings

**Technical Notes** 

Construction Methodology



### Document / Drawing Issue Sheet



Project Title	Carrownagowan WF - 110kV UGC	Project No.	05-6	541										
Т	ïtle	Drawing/ Doc Number	Size					R	evisio	on				
Overall Site	e Layout Plan	05641-200	A1	00	00	01	01							
Site Layout	Plan (1 of 16)	05641-201	A1	00	00	01	01							
Site Layout	Plan (2 of 16)	05641-202	A1	00	00	01	01							
Site Layout	Plan (3 of 16)	05641-203	A1	00	00	01	01							
Site Layout	Plan (4 of 16)	05641-204	A1	00	00	01	01							
Site Layout	Plan (5 of 16)	05641-205	A1	00	00	01	01							
Site Layout	Plan (6 of 16)	05641-206	A1	00	00	01	01							
Site Layout	Plan (7 of 16)	05641-207	A1	00	00	01	01							
Site Layout	Plan (8 of 16)	05641-208	A1	00	00	01	01							
Site Layout	Plan (9 of 16)	05641-209	A1	00	00	01	01							
Site Layout	Plan (10 of 16)	05641-210	A1	00	00	01	01							
Site Layout	Plan (11 of 16)	05641-211	A1	00	00	01	01							
Site Layout	Plan (12 of 16)	05641-212	A1	00	00	01	01							
Site Layout	Plan (13 of 16)	05641-213	A1	00	00	01	01							
Site Layout	Plan (14 of 16)	05641-214	A1	00	00	01	01							
Substation Co	onnections (SLP)	05641-217	A1	00	00	01	01							
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### Document / Drawing Issue Sheet



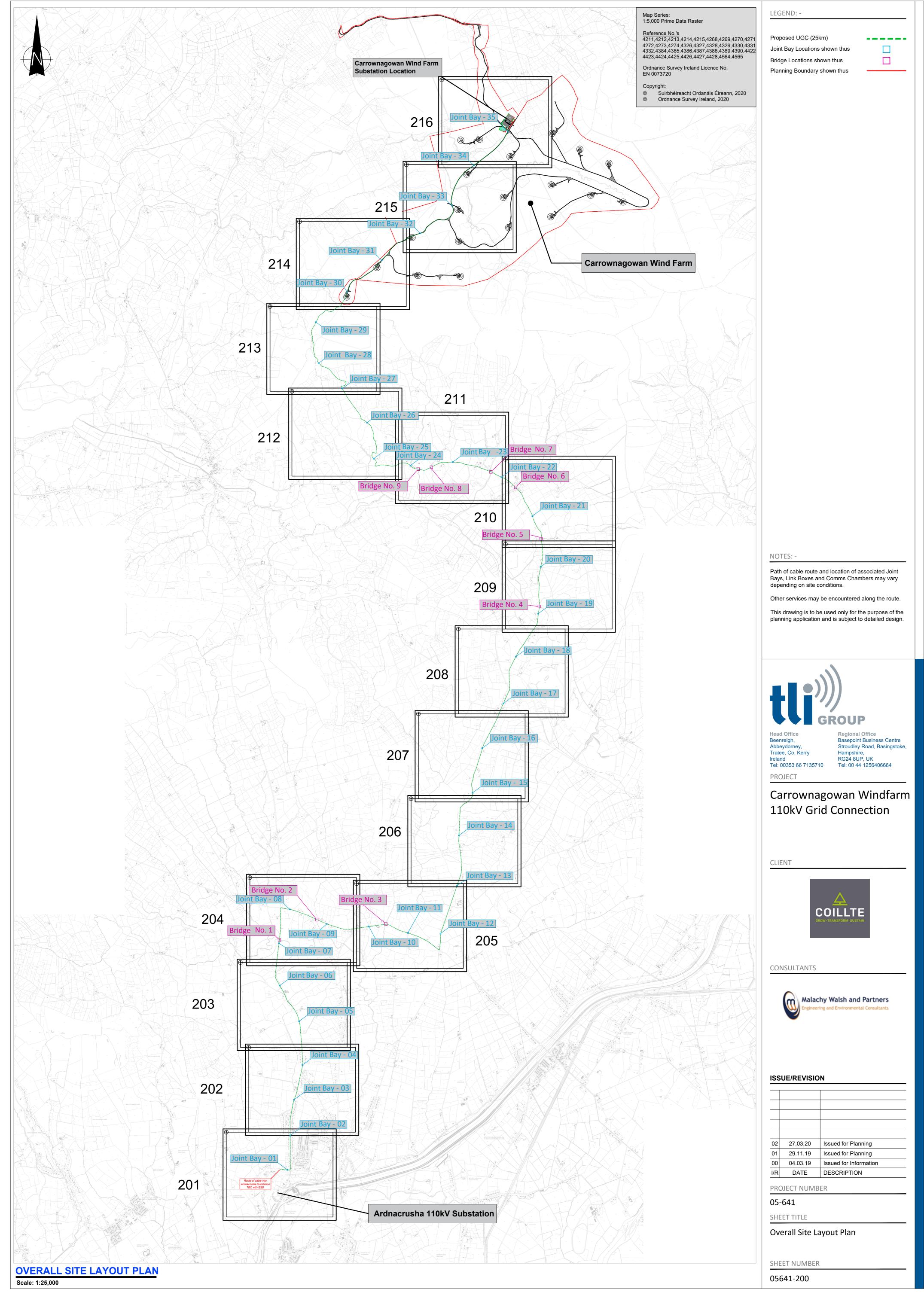
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Typical Ducting R	loadways (Trefoil)	0564	1-222	A1	00	00	01	02					
Typical 110	kV Joint Bay	0564	1-223	A1	00	00	01	02					
Typical Serv	vice Crossing	0564	1-224	A1	00	00	01	02					
Typical Water	main Crossing	0564	1-225	A1	00	00	01	02					
Typical H	DD Detail	0564	1-227	A3	00	00	01	01					
Typical Ducting	Flat Formation	0564	1-229	A3	00	00	01	02					
Typical Ducting	Forestry Roads	0564	1-228	A3	00	00	01	02					
Typical 110kV C	Comms Chamber	0564	1-230	A3	00	00	01	02					
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Bridge C	rossings 2	0564	1-232	A2	00	00	01	01					
Bridge C	rossings 3	0564	1-233	A2	00	00	01	01					
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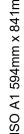
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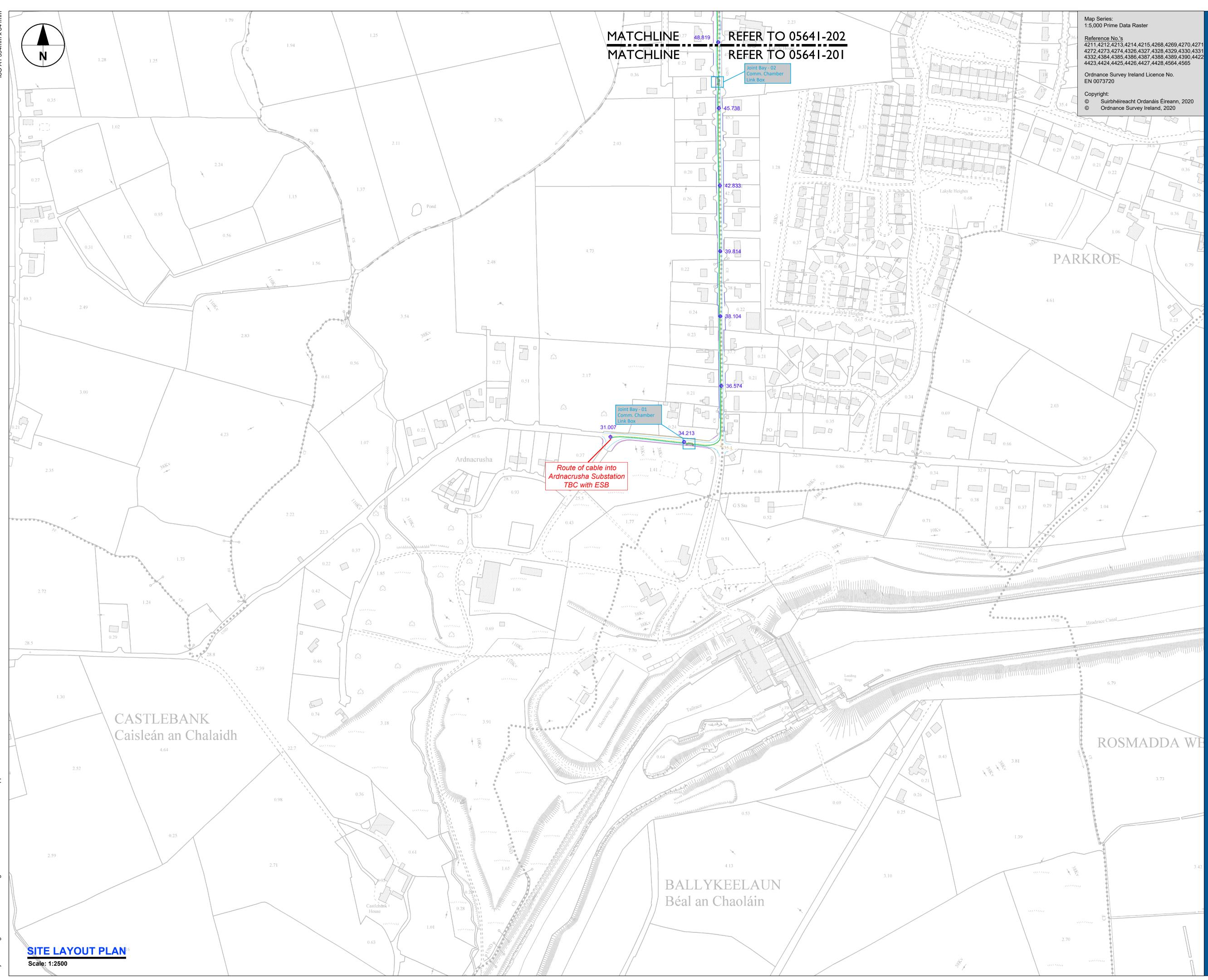


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Bridge (	Crossings 9	05642	L-239	A2	00	00	01	01					
Culvert Cro	ossings 1 of 3	05642	L-240	A2	00	00	01	01					
Culvert Cro	ossings 2 of 3	05642	L-241	A2	00	00	01	01					
Tech Note 2: C	able Rating Check	05641	-TN02	A4	00		00	00					
Tech Note 3: Ca	able Pulling Check	05641	-TN03	A4	00		01	01					
Construction	n Methodology	05641	L-R03	A4	00		01	01					
Joint Bay Su	ummary Sheet	-		-	00		01	01					
Site Layout	Plan (15 of 16)	05642	L-215	A1			00	00					
Site Layout	Plan (16 of 16)	05642	L-216	A1			00	00					
Culvert Cro	ossings 3 of 3	05642	L-242	A2			00	00					
Transition C	Chamber Detail	05642	L-243	A3				00					
Link Box Ch	amber Details	05642	L-244	A3				00					
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### Carrownagowan Wind Farm 110kV Grid Connection

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#### NOTES: -

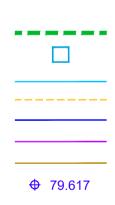
Path of cable route and location of associated Joint Bays, Link Boxes and Comms Chambers may vary depending on site conditions.

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Road Edge shown thus Road Centre shown thus Concrete Wall shown thus Fence Line shown thus Verge shown thus Existing levels shown thus



### **ISSUE/REVISION**

02	27.03.20	Issued for Planning
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05-641

SHEET TITLE

Site Layout Plan Sheet 1 of 16

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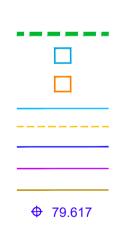
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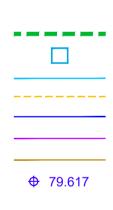
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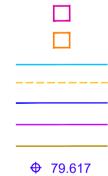
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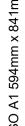
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Site Layout Plan Sheet 4 of 16

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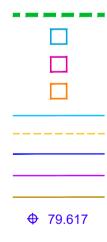
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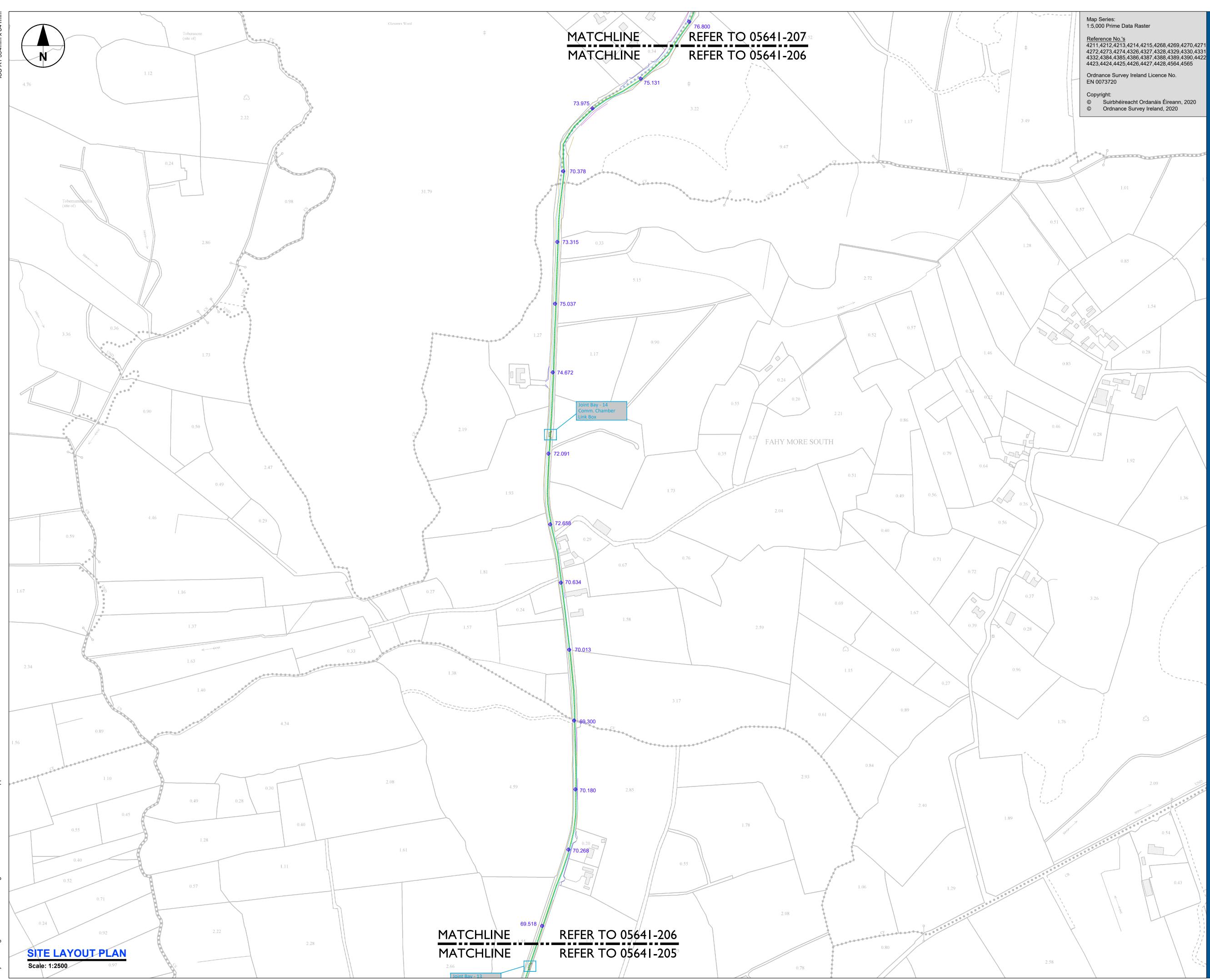
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Site Layout Plan Sheet 5 of 16

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### PROJECT

## Carrownagowan Wind Farm 110kV Grid Connection

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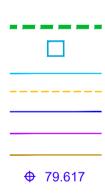
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# Carrownagowan Wind Farm 110kV Grid Connection

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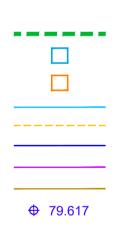
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### PROJECT

Carrownagowan Wind Farm 110kV Grid Connection

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#### NOTES: -

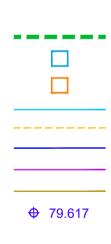
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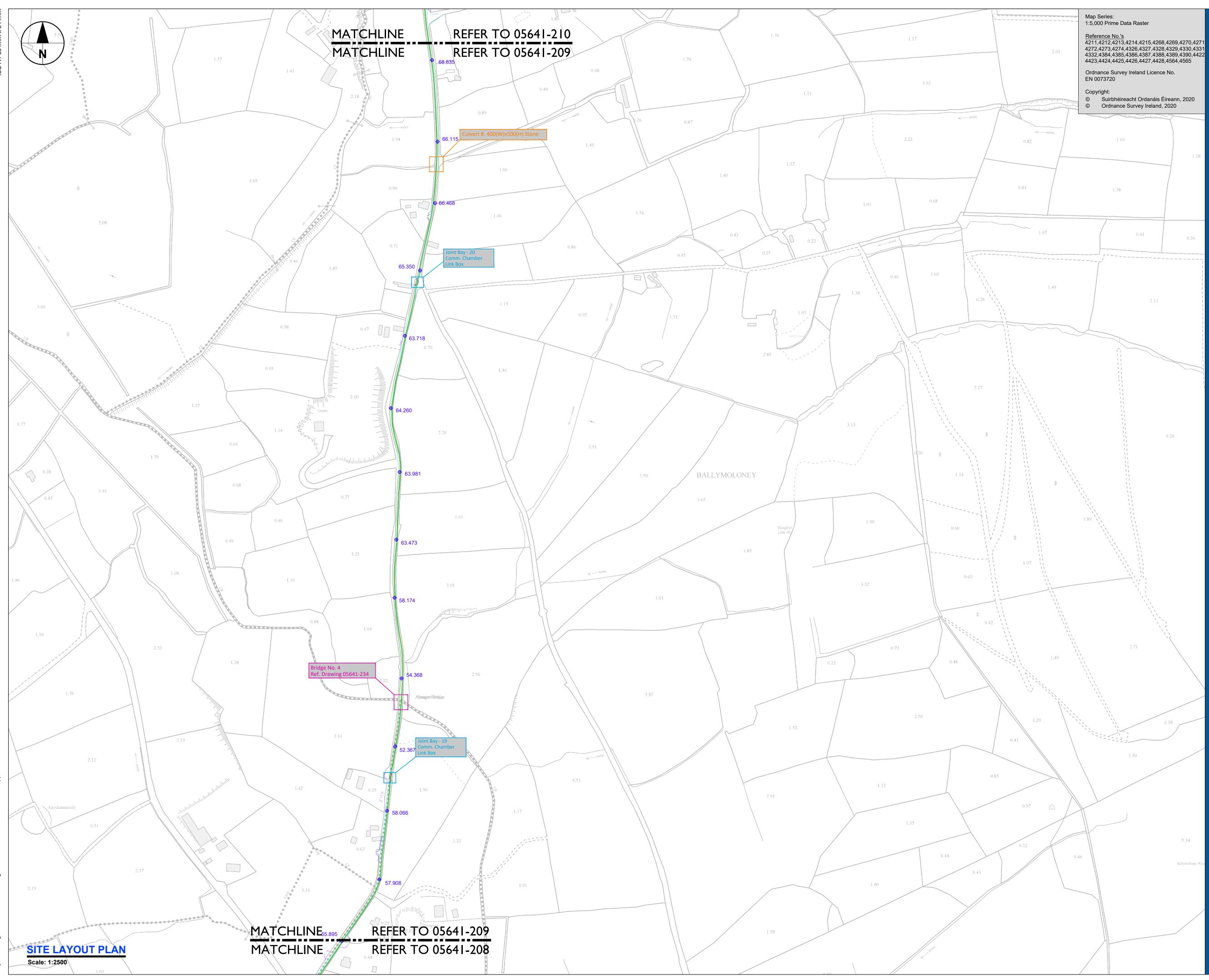
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Site Layout Plan Sheet 8 of 16

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# Carrownagowan Wind Farm 110kV Grid Connection

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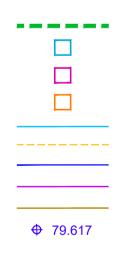
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Site Layout Plan Sheet 9 of 16

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### PROJECT

### Carrownagowan Wind Farm 110kV Grid Connection

### CLIENT



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#### NOTES: -

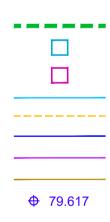
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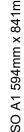
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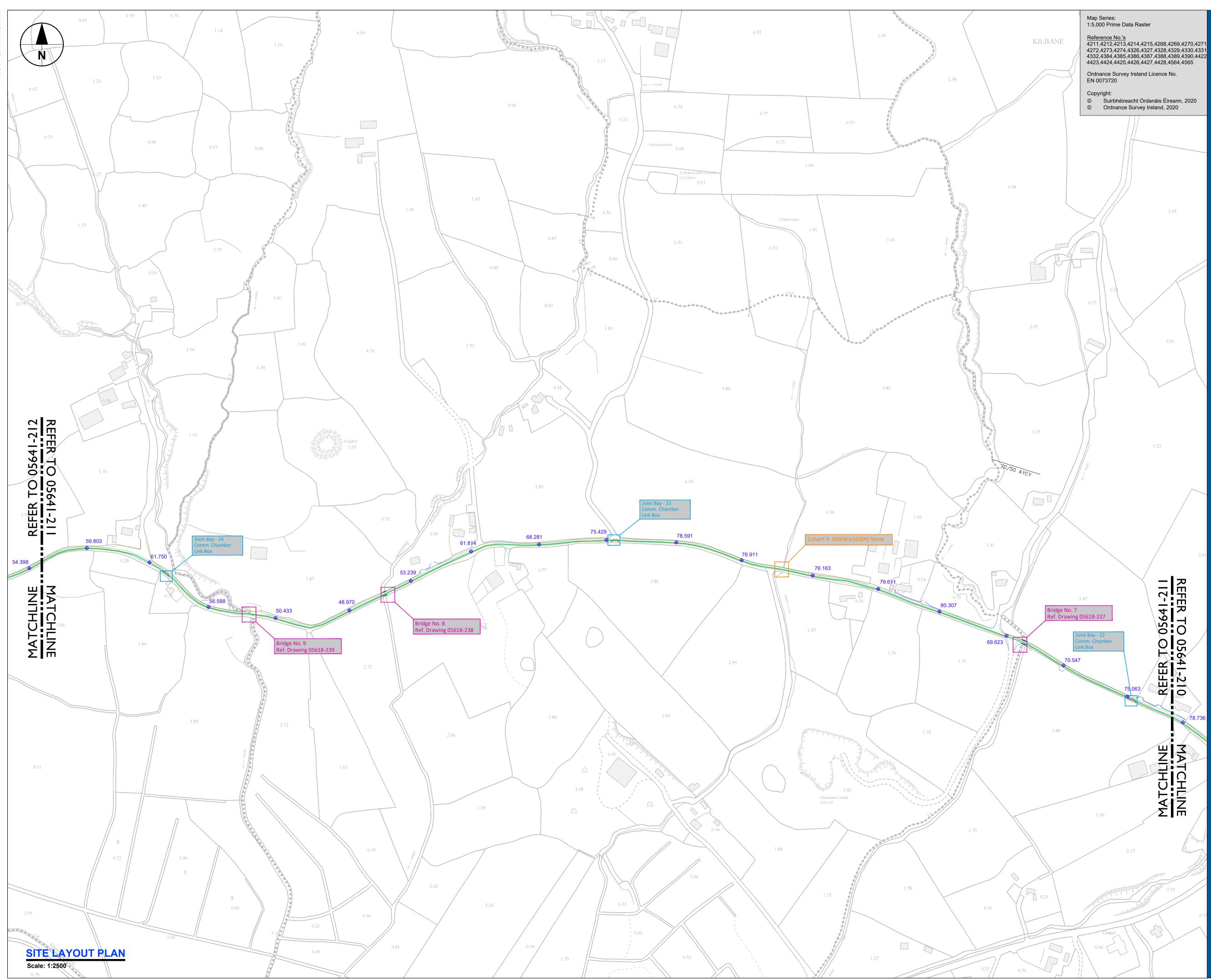
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Site Layout Plan Sheet 10 of 16

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### PROJECT

### Carrownagowan Wind Farm 110kV Grid Connection

### CLIENT



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#### NOTES: -

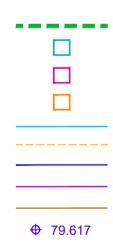
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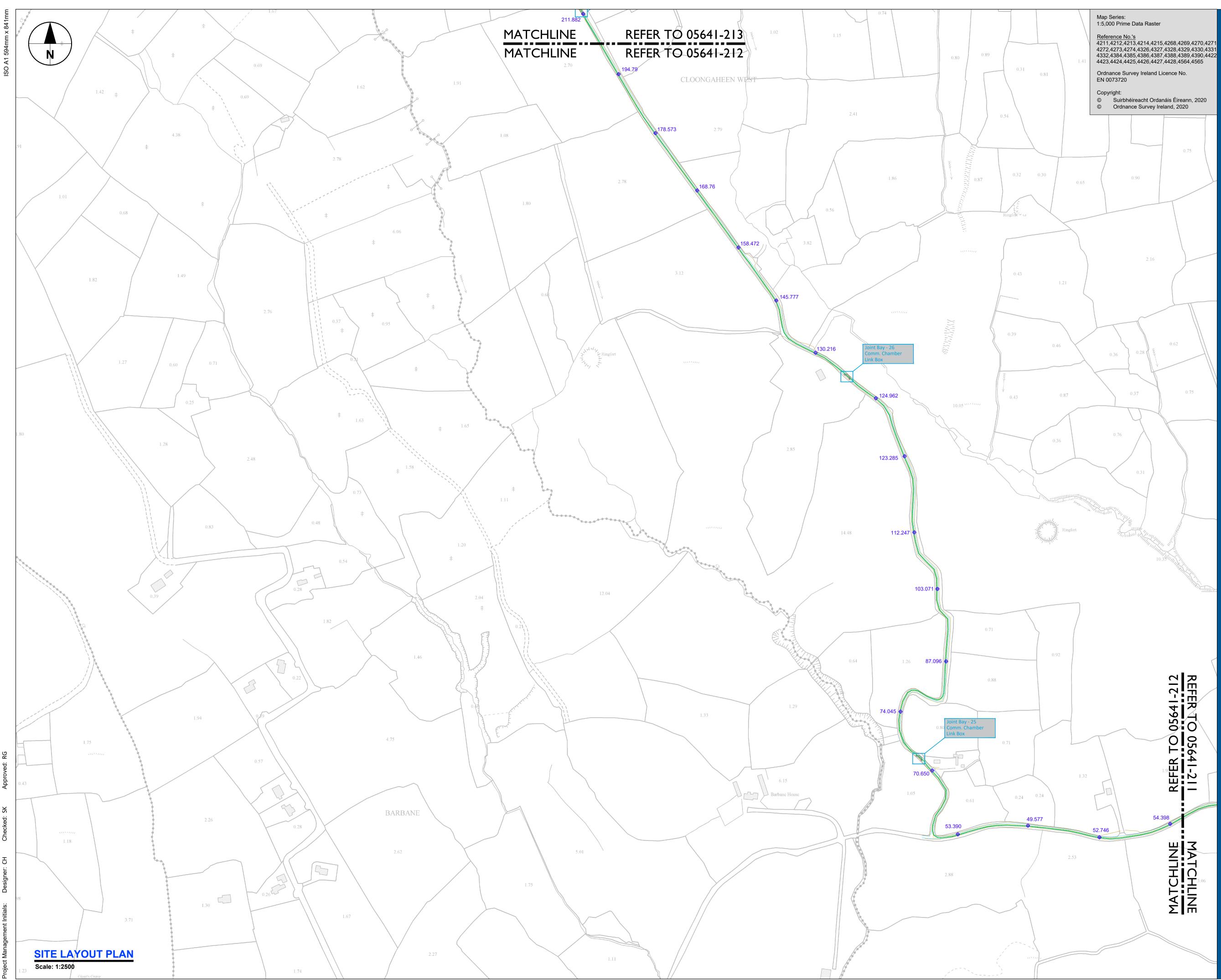
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Site Layout Plan Sheet 11 of 16

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# Carrownagowan Wind Farm 110kV Grid Connection

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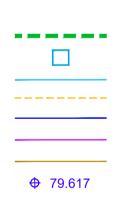
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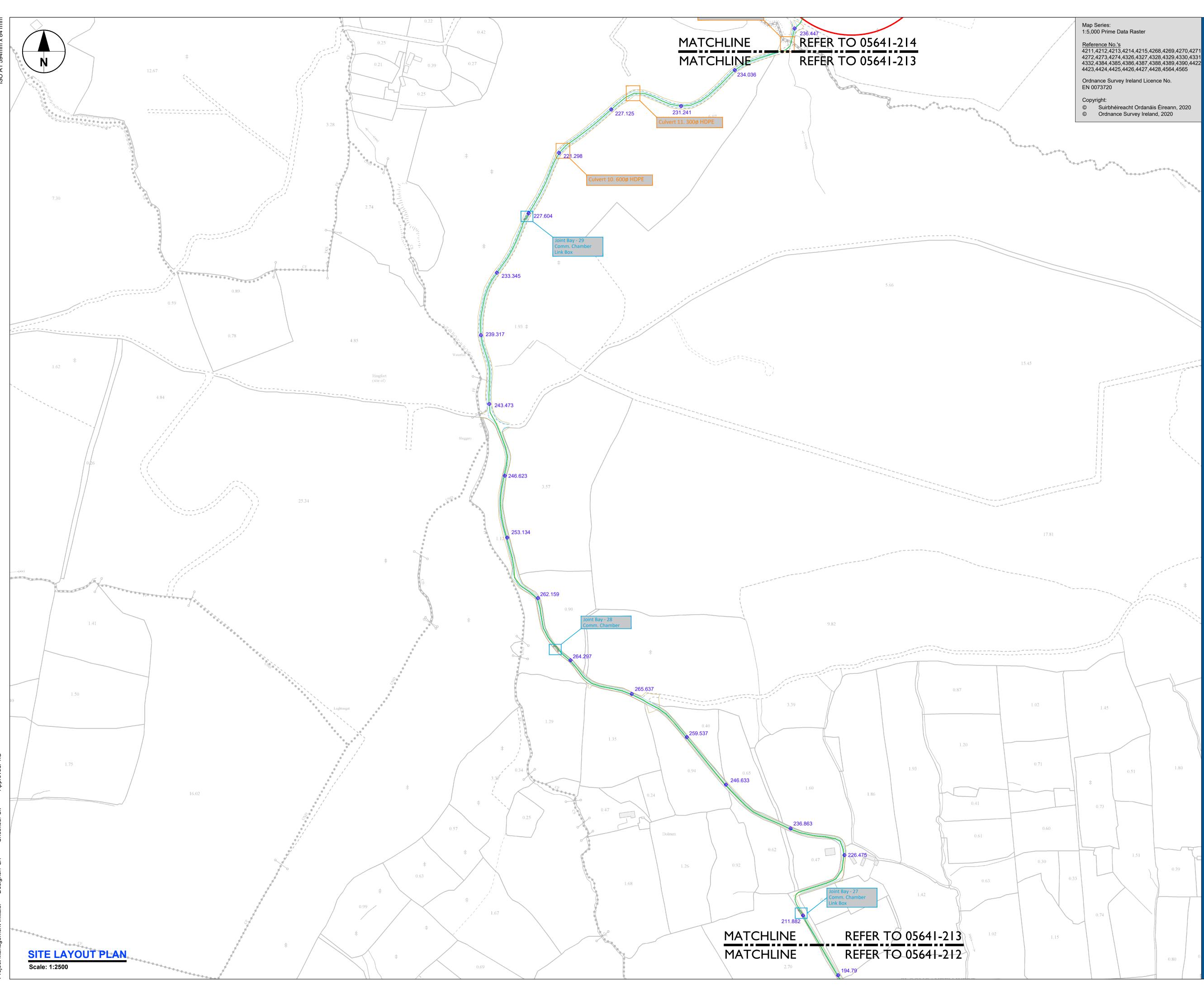
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Site Layout Plan Sheet 12 of 16

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oject Management Initials: Designer: CH Checked: SK Appro

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### PROJECT

## Carrownagowan Wind Farm 110kV Grid Connection

### CLIENT



### CONSULTANTS



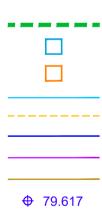
#### NOTES: -

Path of cable route and location of associated Joint Bays, Link Boxes and Comms Chambers may vary depending on site conditions.

Other services may be encountered along the route.

This drawing is to be used only for the purpose of the planning application and is subject to detailed design. LEGEND: -

Proposed UGC (25km) Joint Bay Locations shown thus Culvert Locations shown thus Road Edge shown thus Road Centre shown thus Concrete Wall shown thus Fence Line shown thus Verge shown thus Existing levels shown thus



### **ISSUE/REVISION**

02	27.03.20	Issued for Planning	
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00	04.03.19	Issued for Information	
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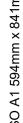
### PROJECT NUMBER

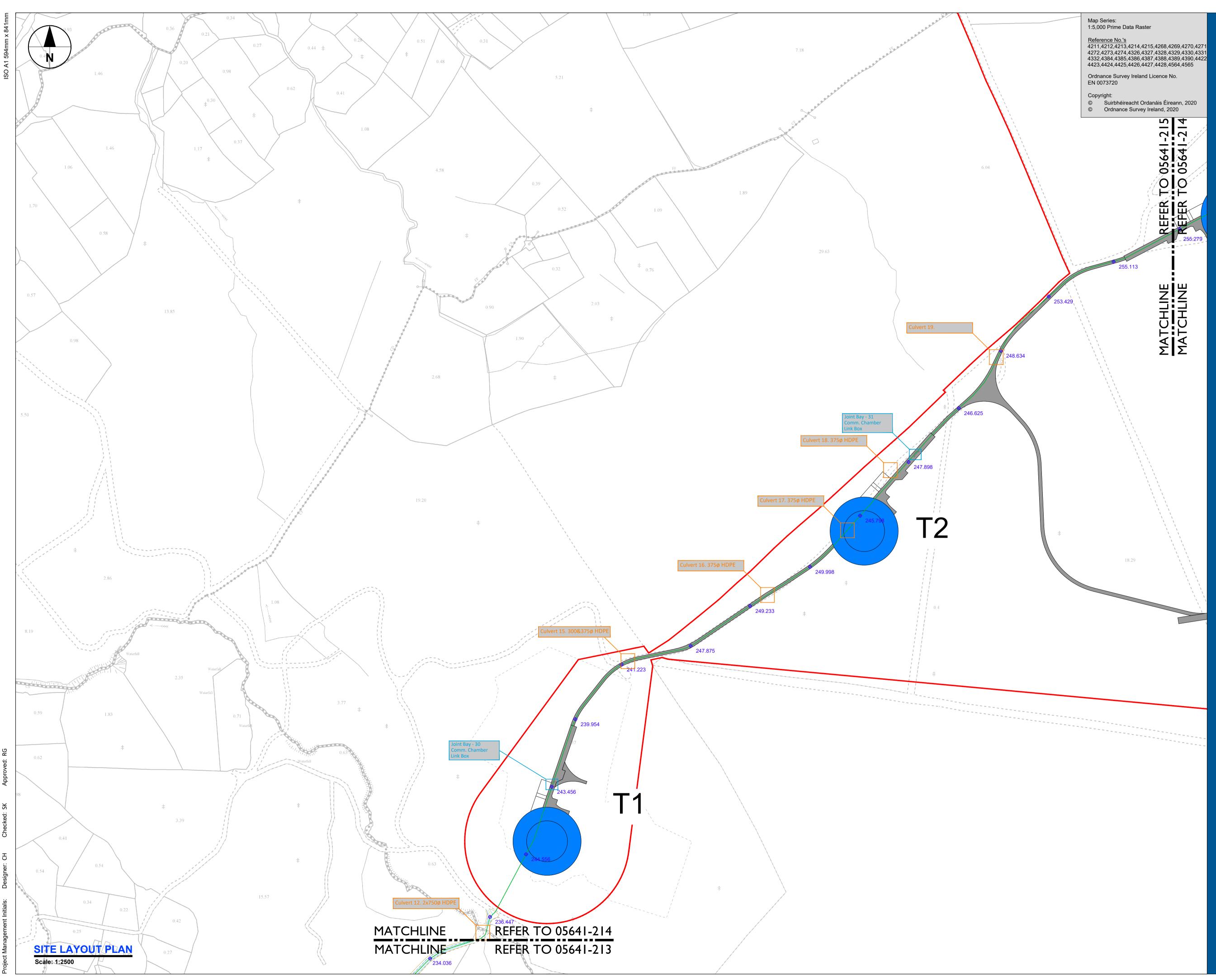
05-641

SHEET TITLE

Site Layout Plan Sheet 13 of 16

SHEET NUMBER





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### PROJECT

### Carrownagowan Wind Farm 110kV Grid Connection

#### CLIENT



#### CONSULTANTS



#### NOTES: -

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This drawing is to be used only for the purpose of the planning application and is subject to detailed design. LEGEND: -

**⊕** 79.617

O T12

Proposed UGC (25km) ----Joint Bay Locations shown thus Culvert Locations shown thus Road Edge shown thus \_\_\_\_\_ Road Centre shown thus Concrete Wall shown thus Fence Line shown thus Verge shown thus Existing levels shown thus Wind Farm roads/hardstandings shown thus Turbine locations shown thus

Wind Farm Planning boundary shown thus

### **ISSUE/REVISION**

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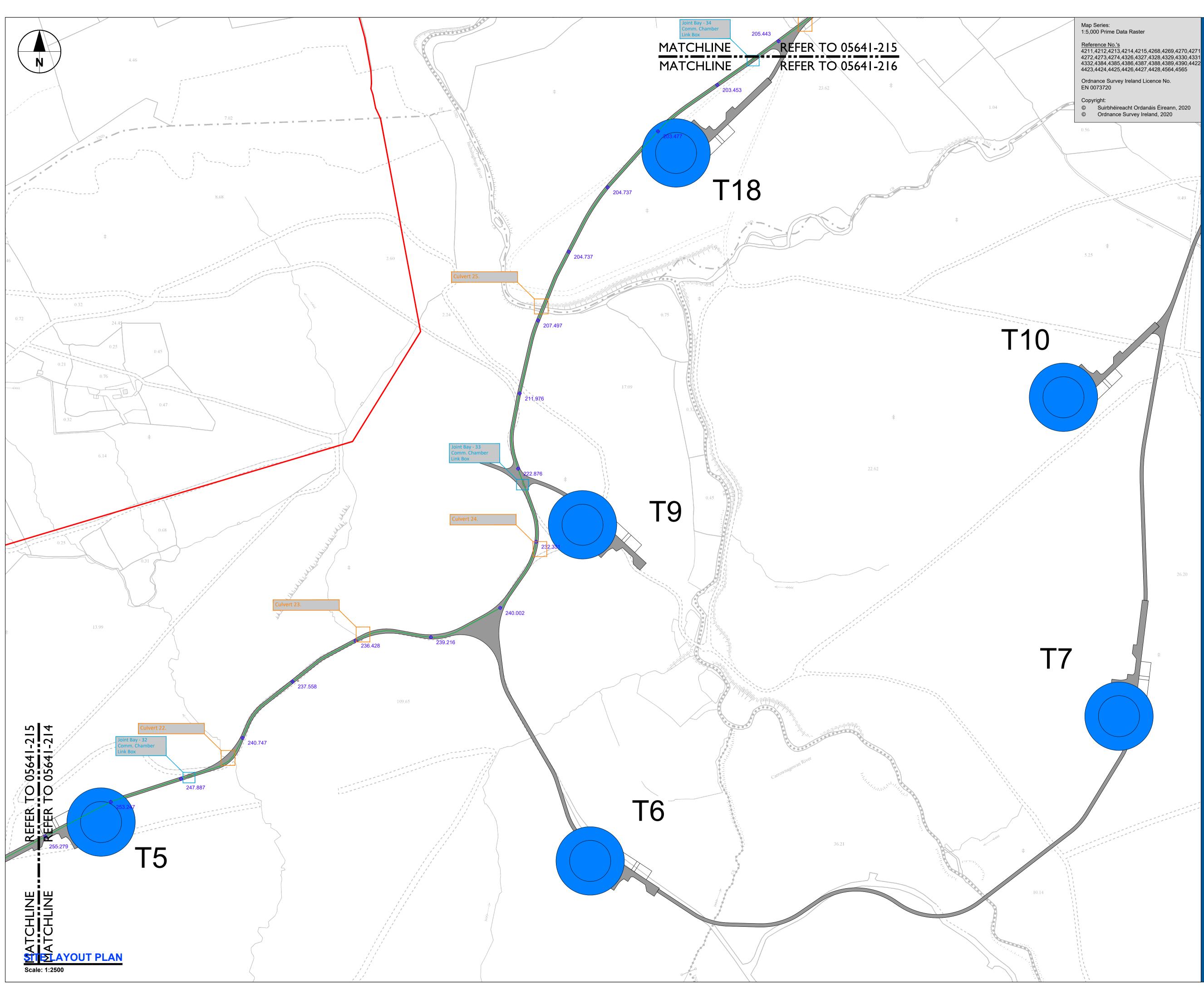
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SHEET TITLE

Site Layout Plan Sheet 14 of 16

SHEET NUMBER





oject Management Initials: Designer: CH Checked: SK Approved: RG



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### PROJECT

Carrownagowan Wind Farm 110kV Grid Connection

### CLIENT



### CONSULTANTS



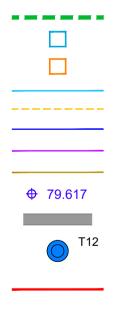
#### NOTES: -

Path of cable route and location of associated Joint Bays, Link Boxes and Comms Chambers may vary depending on site conditions.

Other services may be encountered along the route.

This drawing is to be used only for the purpose of the planning application and is subject to detailed design. LEGEND: -

Proposed UGC (25km) Joint Bay Locations shown thus Culvert Locations shown thus Road Edge shown thus Road Centre shown thus Concrete Wall shown thus Fence Line shown thus Verge shown thus Existing levels shown thus Wind Farm roads/hardstandings shown thus Turbine locations shown thus



### **ISSUE/REVISION**

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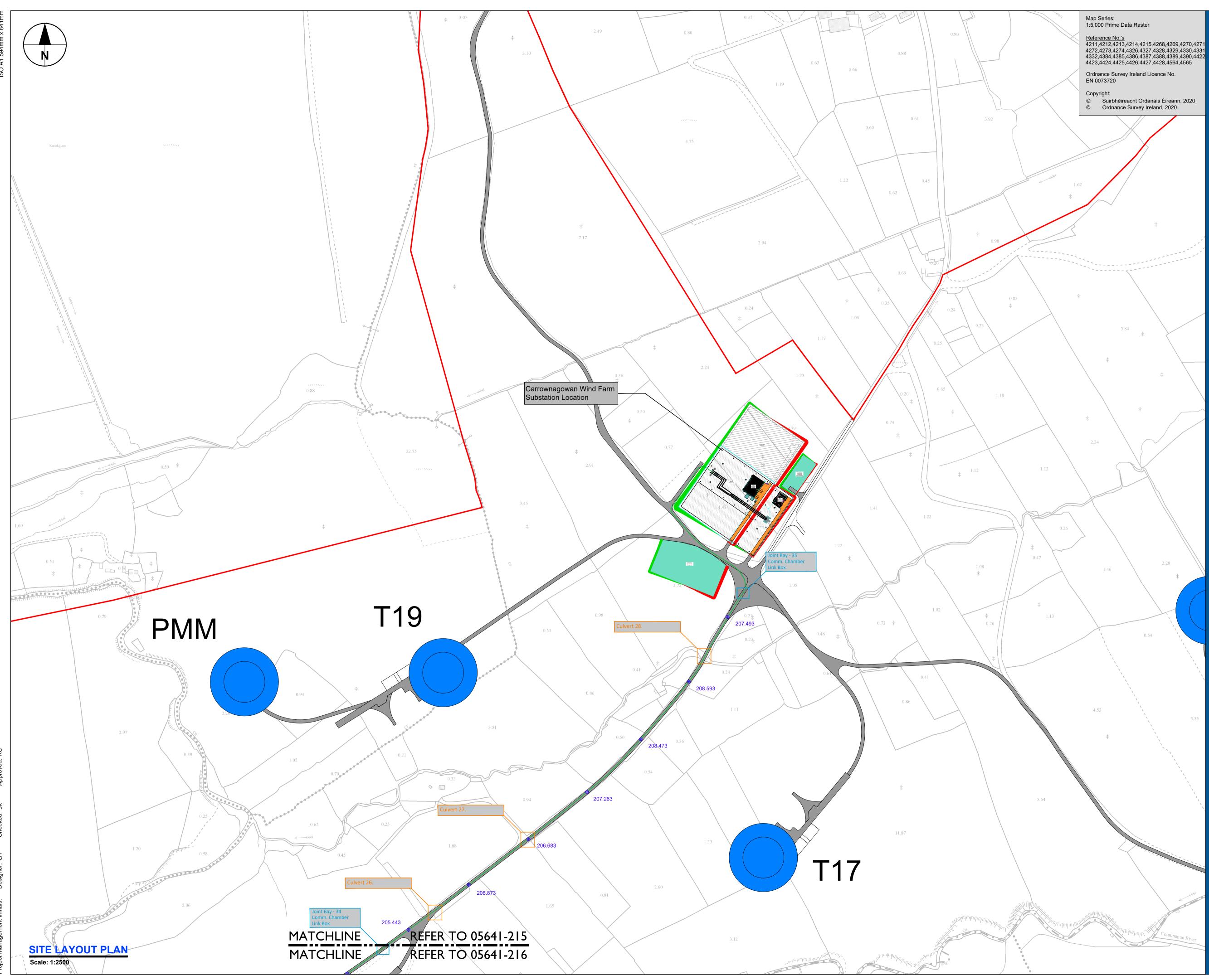
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SHEET TITLE

Site Layout Plan Sheet 15 of 16

SHEET NUMBER





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### PROJECT

## Carrownagowan Wind Farm 110kV Grid Connection

### CLIENT



### CONSULTANTS



#### NOTES: -

Path of cable route and location of associated Joint Bays, Link Boxes and Comms Chambers may vary depending on site conditions.

Other services may be encountered along the route.

This drawing is to be used only for the purpose of the planning application and is subject to detailed design. LEGEND: -

Proposed UGC (25km) Joint Bay Locations shown thus Culvert Locations shown thus Road Edge shown thus Road Centre shown thus Concrete Wall shown thus Fence Line shown thus Verge shown thus Existing levels shown thus Wind Farm roads/hardstandings shown thus Turbine locations shown thus Wind Farm Planning boundary shown thus



### **ISSUE/REVISION**

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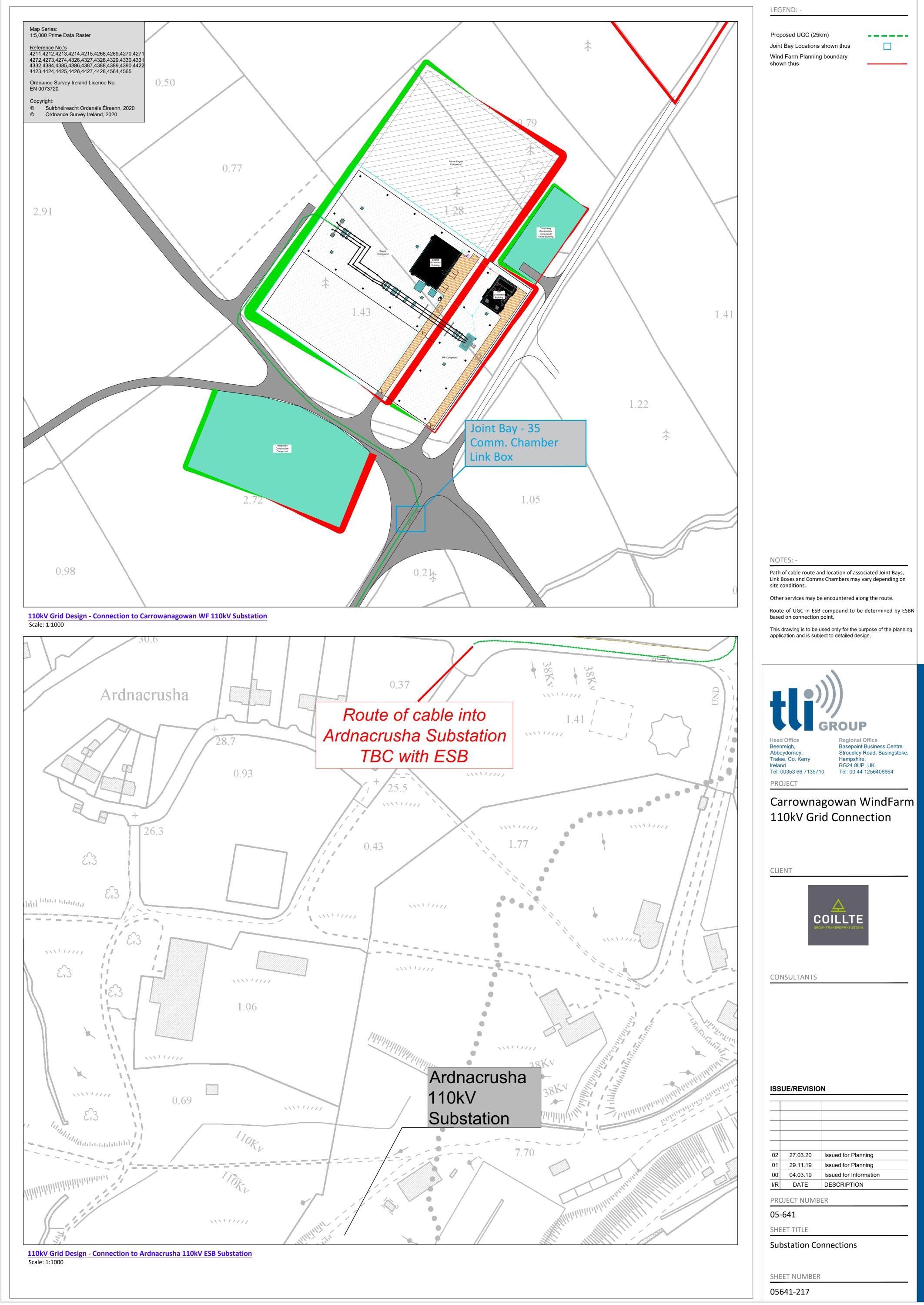
### PROJECT NUMBER

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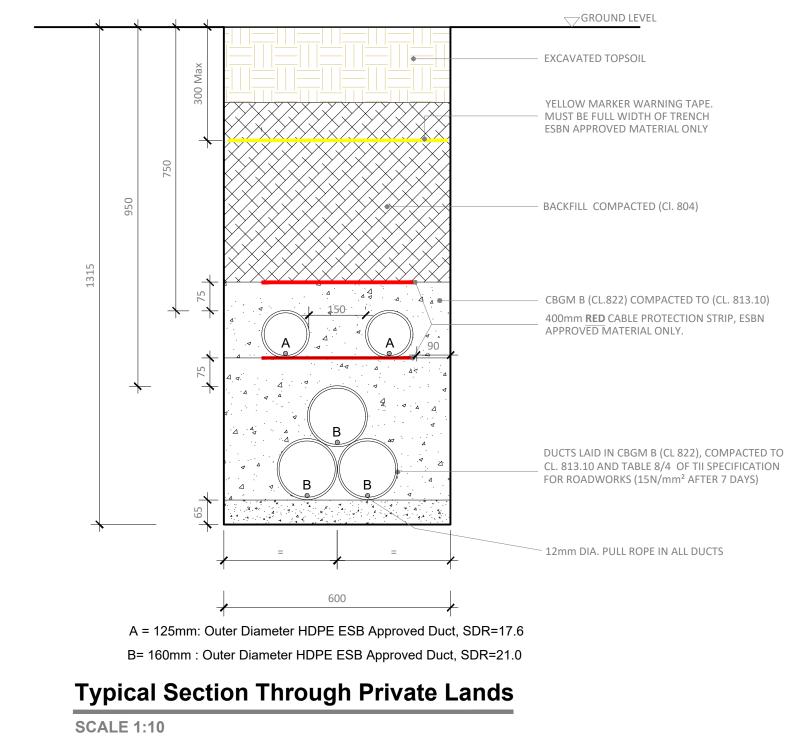
SHEET TITLE

Site Layout Plan Sheet 16 of 16

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ISO A1 594mm x 841mm

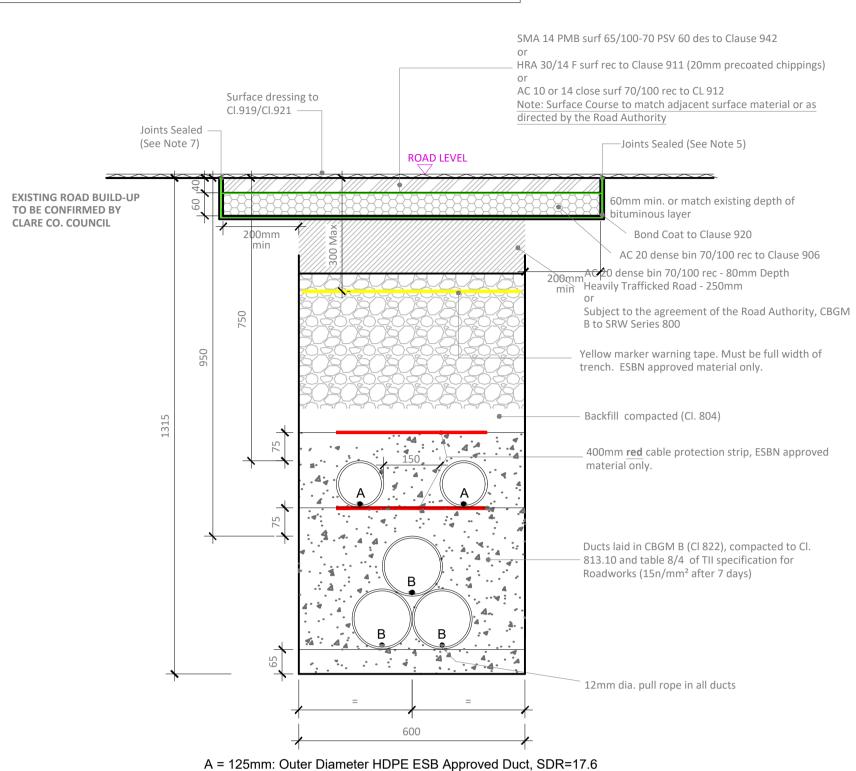




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### **Permanent Reinstatement**





B= 160mm : Outer Diameter HDPE ESB Approved Duct, SDR= 21

Typical Section Through Permanent Reinstatement of Longitudinal **Opening in Roadway** 

**SCALE 1:10** 

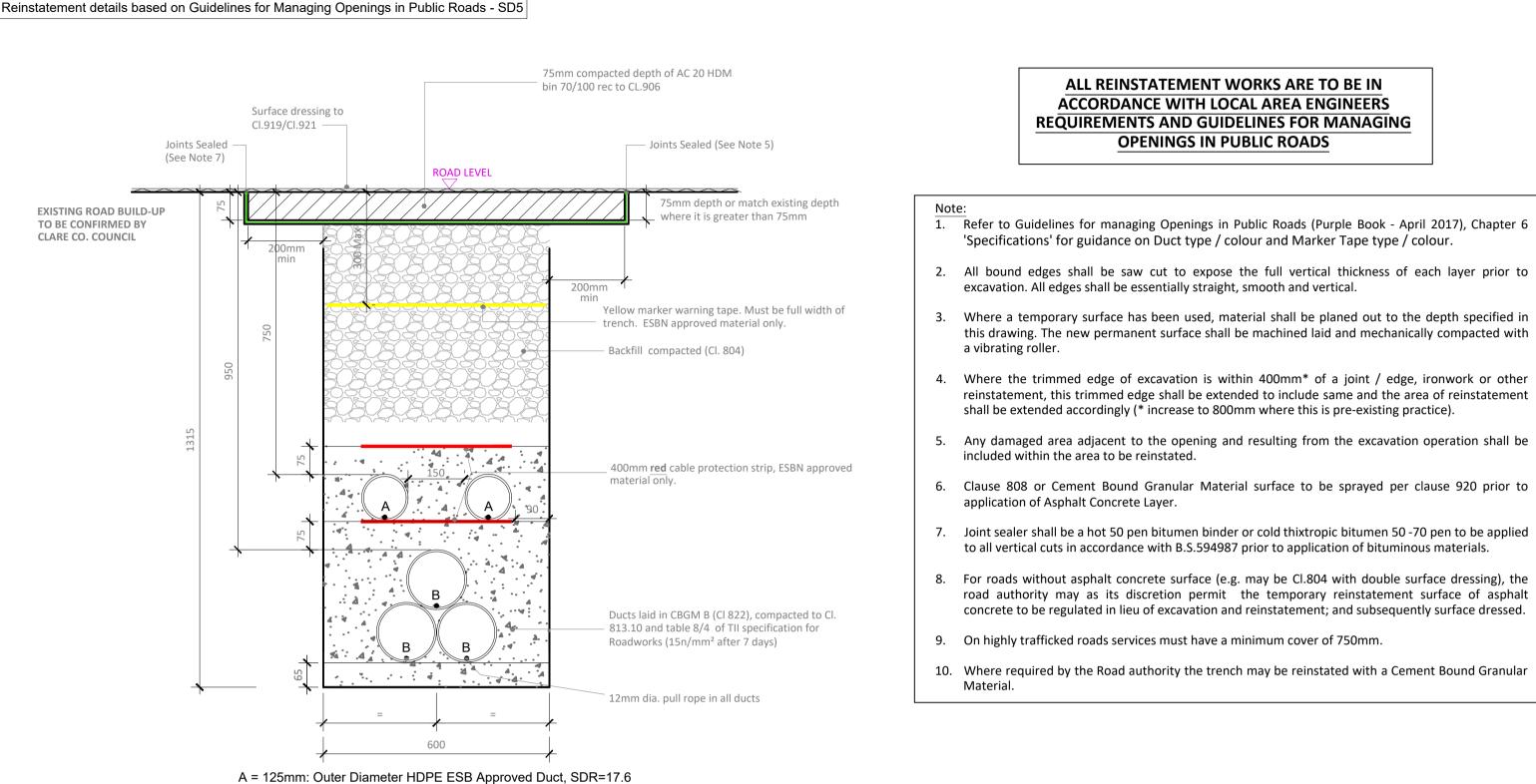
### **Temporary Reinstatement**

Reinstatement details based on Guidelines for Managing Openings in Public Roads - SD1

AC 20 Dense bin 70/100 rec - Depth: 100mm or 50mm compacted depth of 14mm (nominal size) cold laid Bitmac to IS EN 13108 (delay set) - only with the road authority's approval Joints Sealed -See Note 4 ROAD LEVEL EXISTING ROAD BUILD-UP TO BE CONFIRMED BY **CLARE CO. COUNCIL** AC 20 dense bin 70/100 rec - 80mm Depth Heavily Trafficked Road - 250mm Subject to the agreement of the Road Authority, CBGM B to SRW Series 800 Yellow marker warning tape. Must be full width of trench. ESBN approved material only. - Backfill compacted (Cl. 804) 400mm red cable protection strip, ESBN approved material only. Ducts laid in CBGM B (Cl 822), compacted to Cl. 813.10 and table 8/4 of TII specification for Roadworks (15n/mm<sup>2</sup> after 7 days) 2 <sup>–</sup> 12mm dia. pull rope in all ducts 600 A = 125mm: Outer Diameter HDPE ESB Approved Duct, SDR=17.6 B= 160mm : Outer Diameter HDPE ESB Approved Duct, SDR= 21

**Typical Section Through Temporary Reinstatement of Longitudinal Opening in Roadway** 

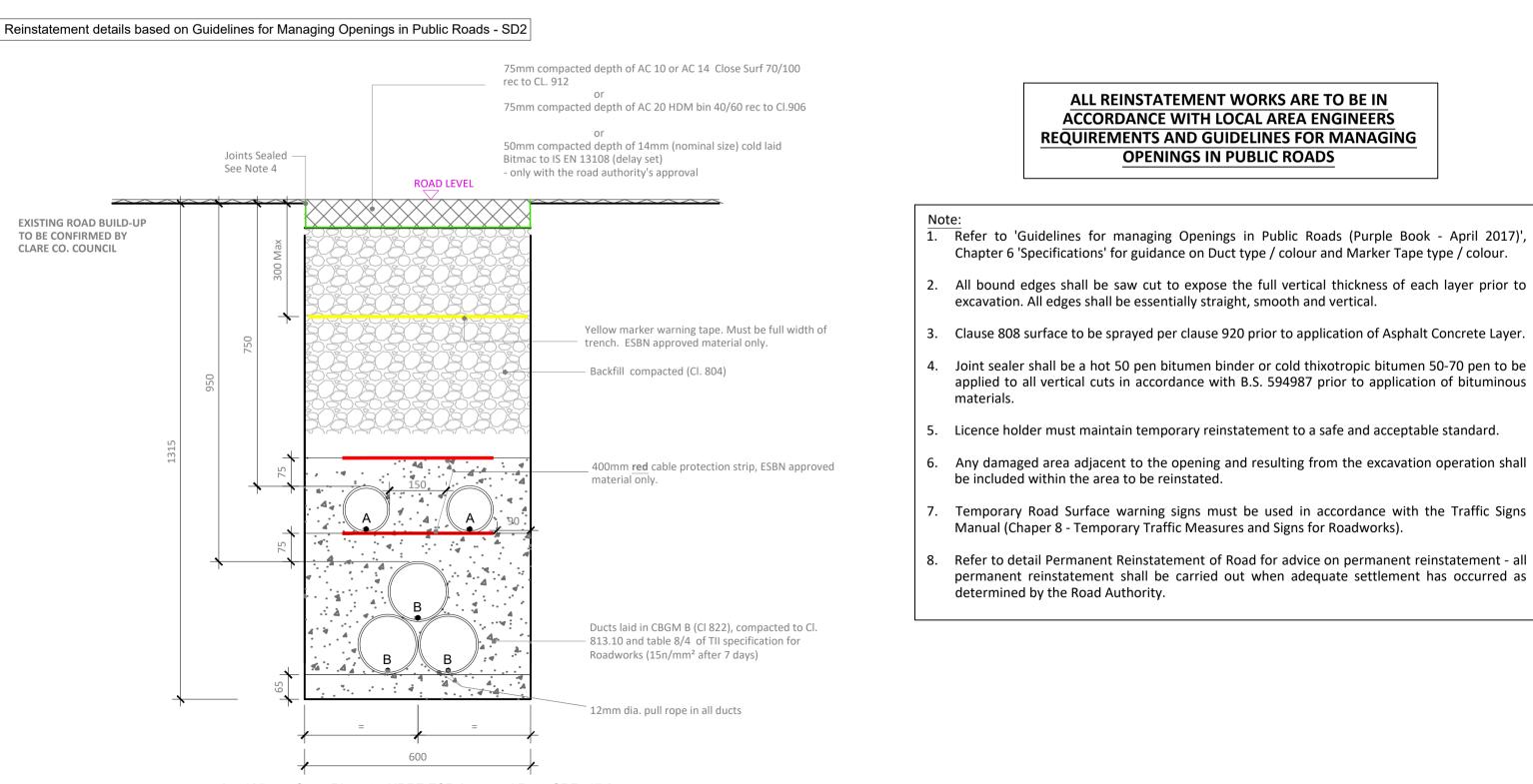




B= 160mm : Outer Diameter HDPE ESB Approved Duct, SDR= 21

### Typical Section Through Permanent Reinstatement of Longitudinal **Opening in Dressed Rural Unbound Roadway**

**SCALE 1:10** 



A = 125mm: Outer Diameter HDPE ESB Approved Duct, SDR=17.6 B= 160mm : Outer Diameter HDPE ESB Approved Duct, SDR= 21

### Typical Section Through Temporary Reinstatement of Longitudinal **Opening in Dressed Rural Unbound Roadway**

### **ACCORDANCE WITH LOCAL AREA ENGINEERS OPENINGS IN PUBLIC ROADS**

1. Refer to Guidelines for managing Openings in Public Roads (Purple Book - April 2017), Chapter 6

3. Where a temporary surface has been used, material shall be planed out to the depth specified in this drawing. The new permanent surface shall be machined laid and mechanically compacted with

. Where the trimmed edge of excavation is within 400mm\* of a joint / edge, ironwork or other reinstatement, this trimmed edge shall be extended to include same and the area of reinstatement

5. Any damaged area adjacent to the opening and resulting from the excavation operation shall be

6. Clause 808 or Cement Bound Granular Material surface to be sprayed per clause 920 prior to

7. Joint sealer shall be a hot 50 pen bitumen binder or cold thixtropic bitumen 50 -70 pen to be applied to all vertical cuts in accordance with B.S.594987 prior to application of bituminous materials.

8. For roads without asphalt concrete surface (e.g. may be Cl.804 with double surface dressing), the road authority may as its discretion permit the temporary reinstatement surface of asphalt concrete to be regulated in lieu of excavation and reinstatement; and subsequently surface dressed.

10. Where required by the Road authority the trench may be reinstated with a Cement Bound Granular

#### ALL REINSTATEMENT WORKS ARE TO BE IN ACCORDANCE WITH LOCAL AREA ENGINEERS **REQUIREMENTS AND GUIDELINES FOR MANAGING OPENINGS IN PUBLIC ROADS**

1. Refer to 'Guidelines for managing Openings in Public Roads (Purple Book - April 2017)', Chapter 6 'Specifications' for guidance on Duct type / colour and Marker Tape type / colour.

applied to all vertical cuts in accordance with B.S. 594987 prior to application of bituminous

5. Licence holder must maintain temporary reinstatement to a safe and acceptable standard.

6. Any damaged area adjacent to the opening and resulting from the excavation operation shall

Temporary Road Surface warning signs must be used in accordance with the Traffic Signs

8. Refer to detail Permanent Reinstatement of Road for advice on permanent reinstatement - all permanent reinstatement shall be carried out when adequate settlement has occurred as

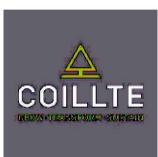


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PROJECT

# Carrownagowan Windfarm 110kV Grid Connection

### CLIENT



### CONSULTANTS



### NOTES: -

- This drawing is to be read in conjunction with relevant drawings, specifications and reports
- Dimensions are in millimeters, unless noted otherwise
- Drawings are not to be scaled use figured
- dimensions only Geogrid may be implemented along the cable trench route where deemed necessary by the contractor or as required by Clare County Council

LEGEND: -

### **ISSUE/REVISION**

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01	29.11.19	Issued for Planning
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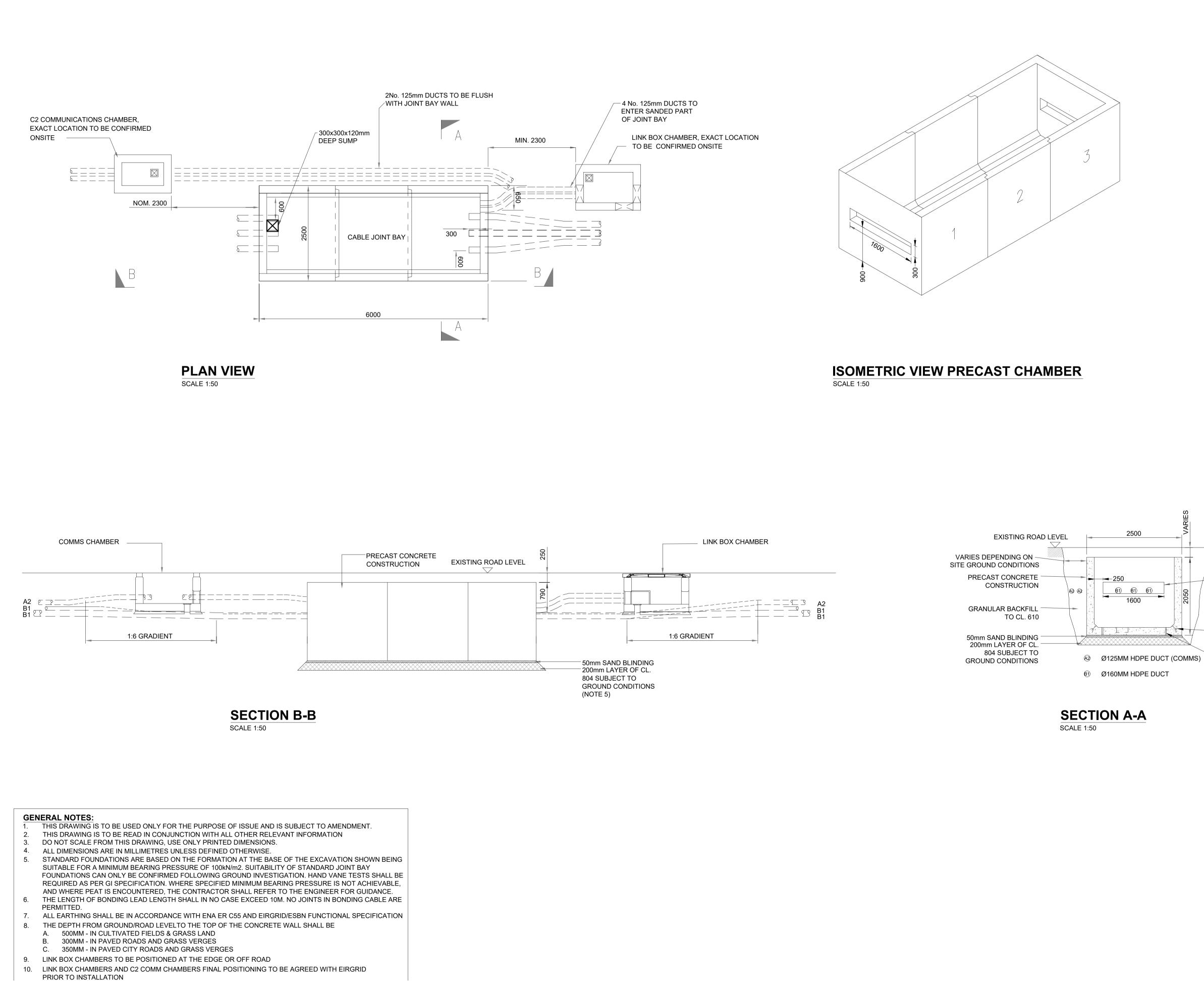
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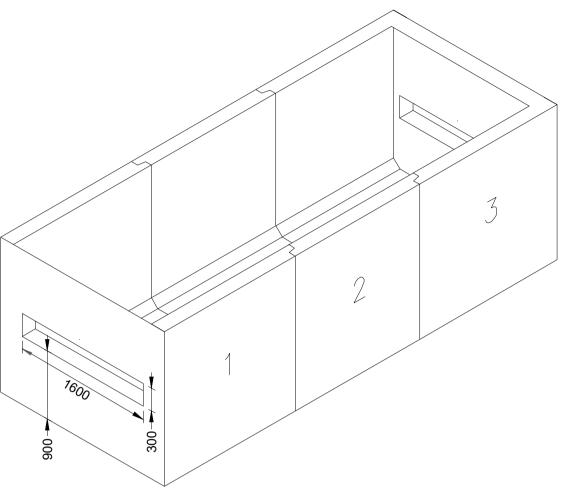
05-641

SHEET TITLE

### Typical Ducting Through Regional / Local Roadways

#### SHEET NUMBER







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PROJECT

# Carrownagowan Wind Farm 110kV Grid Connection

CLIENT



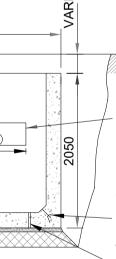
CONSULTANTS



NOTES: -

See General Notes

LEGEND: -



AFTER PLACING THE DUCTS VOID IS TO BE PACKED WITH - CONCRETE C16/20 CONTAINING A NON-SHRINK ADDITIVE BY EIRGRID

10 T HALFEN DEHA \_ SPHERICAL LIFTING ANCHORS. REF: 6000-10.0-0170 4 PER UNIT

30mmØ OPENING IN SLAB

#### **ISSUE/REVISION**

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#### **PROJECT NUMBER**

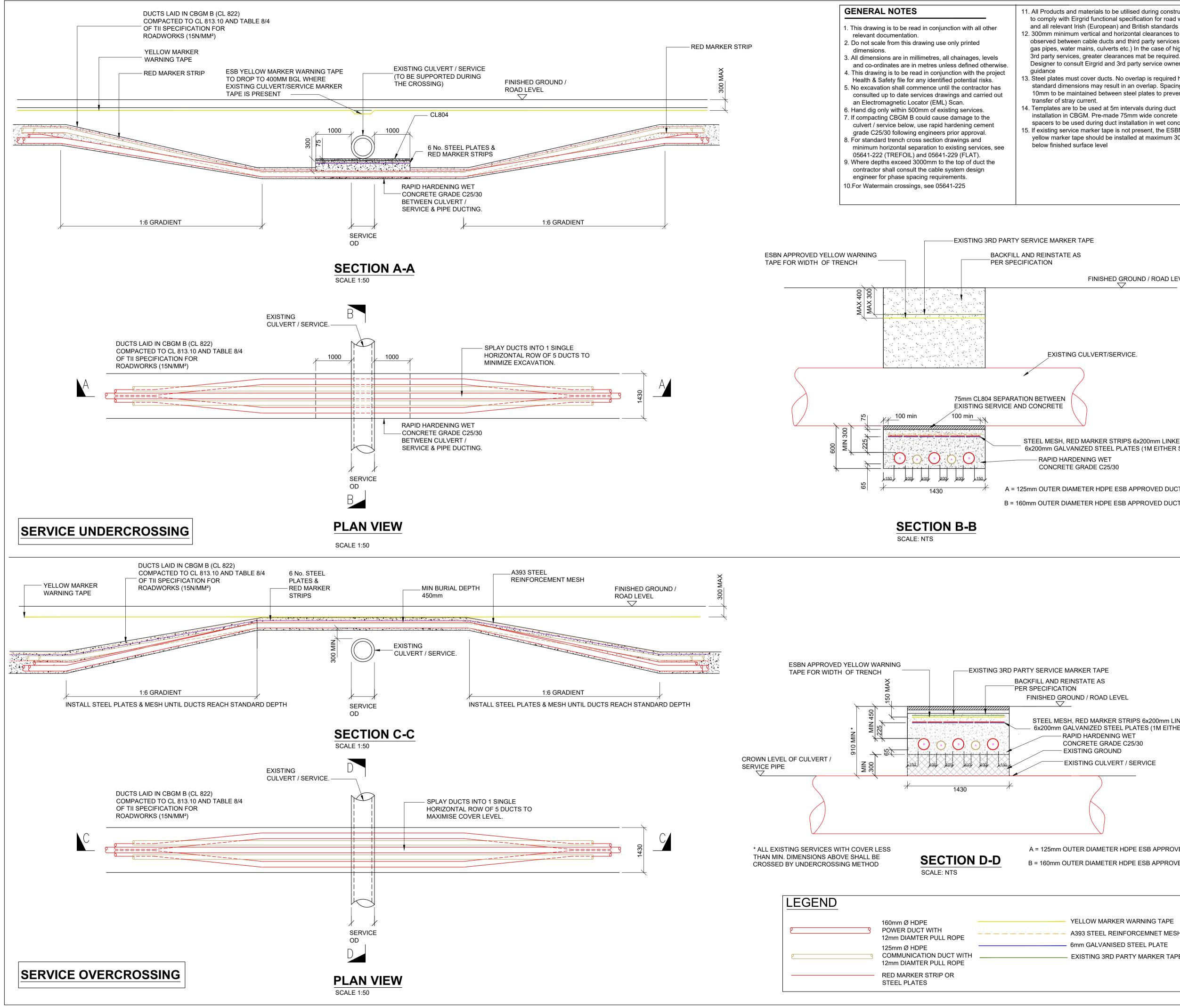
05-641

SHEET TITLE

### 110kV Joint Bay General Arrangement and Details

SHEET NUMBER





11. All Products and materials to be utilised during construction to comply with Eirgrid functional specification for road works and all relevant Irish (European) and British standards 12. 300mm minimum vertical and horizontal clearances to be observed between cable ducts and third party services (e.g. gas pipes, water mains, culverts etc.) In the case of high risk 3rd party services, greater clearances mat be required. Designer to consult Eirgrid and 3rd party service owners for

13. Steel plates must cover ducts. No overlap is required however standard dimensions may result in an overlap. Spacing of 10mm to be maintained between steel plates to prevent the

installation in CBGM. Pre-made 75mm wide concrete spacers to be used during duct installation in wet concrete 15. If existing service marker tape is not present, the ESBN yellow marker tape should be installed at maximum 300mm

FINISHED GROUND / ROAD LEVEL

STEEL MESH, RED MARKER STRIPS 6x200mm LINKED TO 6x200mm GALVANIZED STEEL PLATES (1M EITHER SIDE OF SERVICE)

A = 125mm OUTER DIAMETER HDPE ESB APPROVED DUCT, SDR=17.6 B = 160mm OUTER DIAMETER HDPE ESB APPROVED DUCT, SDR=21

STEEL MESH, RED MARKER STRIPS 6x200mm LINKED TO 6x200mm GALVANIZED STEEL PLATES (1M EITHER SIDE OF SERVICE) - RAPID HARDENING WET CONCRETE GRADE C25/30

EXISTING CULVERT / SERVICE

A = 125mm OUTER DIAMETER HDPE ESB APPROVED DUCT, SDR=17.6 B = 160mm OUTER DIAMETER HDPE ESB APPROVED DUCT, SDR=21

> YELLOW MARKER WARNING TAPE A393 STEEL REINFORCEMNET MESH 6mm GALVANISED STEEL PLATE EXISTING 3RD PARTY MARKER TAPE



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PROJECT

### Carrownagowan Wind Farm 110kV Grid Connection

CLIENT



CONSULTANTS



(m) Malachy Walsh and Partners Engineering and Environmental Consultants

NOTES: -

See General Notes

LEGEND: -

### **ISSUE/REVISION**

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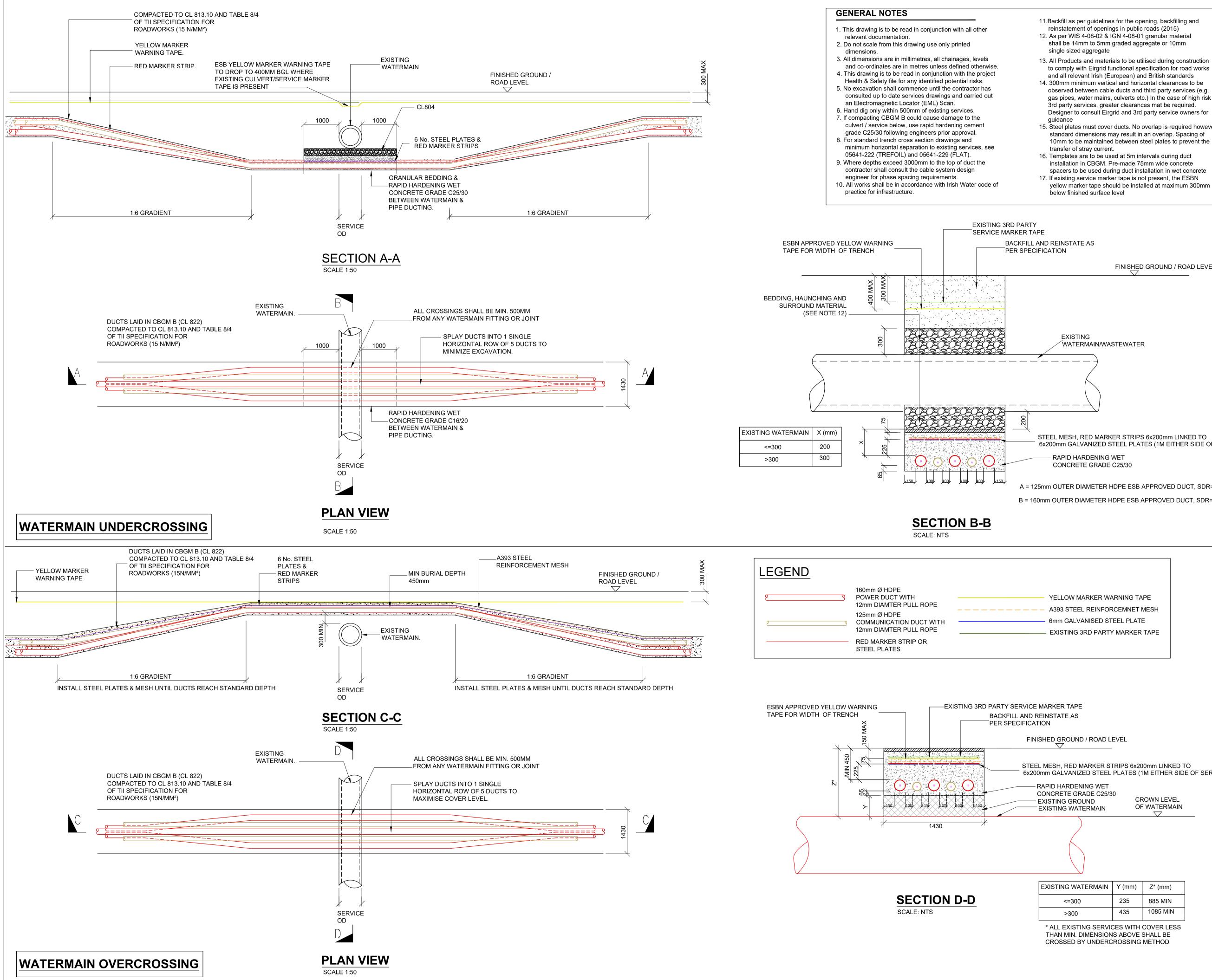
### **PROJECT NUMBER**

05-641

SHEET TITLE

Typical Trench Sections for Crossing Existing Culverts/Services

### SHEET NUMBER



11.Backfill as per guidelines for the opening, backfilling and reinstatement of openings in public roads (2015) 12. As per WIS 4-08-02 & IGN 4-08-01 granular material shall be 14mm to 5mm graded aggregate or 10mm

to comply with Eirgrid functional specification for road works and all relevant Irish (European) and British standards 14. 300mm minimum vertical and horizontal clearances to be observed between cable ducts and third party services (e.g. gas pipes, water mains, culverts etc.) In the case of high risk 3rd party services, greater clearances mat be required. Designer to consult Eirgrid and 3rd party service owners for

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installation in CBGM. Pre-made 75mm wide concrete spacers to be used during duct installation in wet concrete 17. If existing service marker tape is not present, the ESBN yellow marker tape should be installed at maximum 300mm

FINISHED GROUND / ROAD LEVEL

STEEL MESH, RED MARKER STRIPS 6x200mm LINKED TO 6x200mm GALVANIZED STEEL PLATES (1M EITHER SIDE OF SER'

A = 125mm OUTER DIAMETER HDPE ESB APPROVED DUCT, SDR=17.6 B = 160mm OUTER DIAMETER HDPE ESB APPROVED DUCT, SDR=21

6x200mm GALVANIZED STEEL PLATES (1M EITHER SIDE OF SERVICE)

**CROWN LEVEL** OF WATERMAIN

G WATERMAIN	Y (mm)	Z* (mm)	
<=300	235	885 MIN	
>300	435	1085 MIN	



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PROJECT

### Carrownagowan Wind Farm 110kV Grid Connection

CLIENT



CONSULTANTS



Malachy Walsh and Partners Engineering and Environmental Consultants

NOTES: -

See General Notes

LEGEND: -

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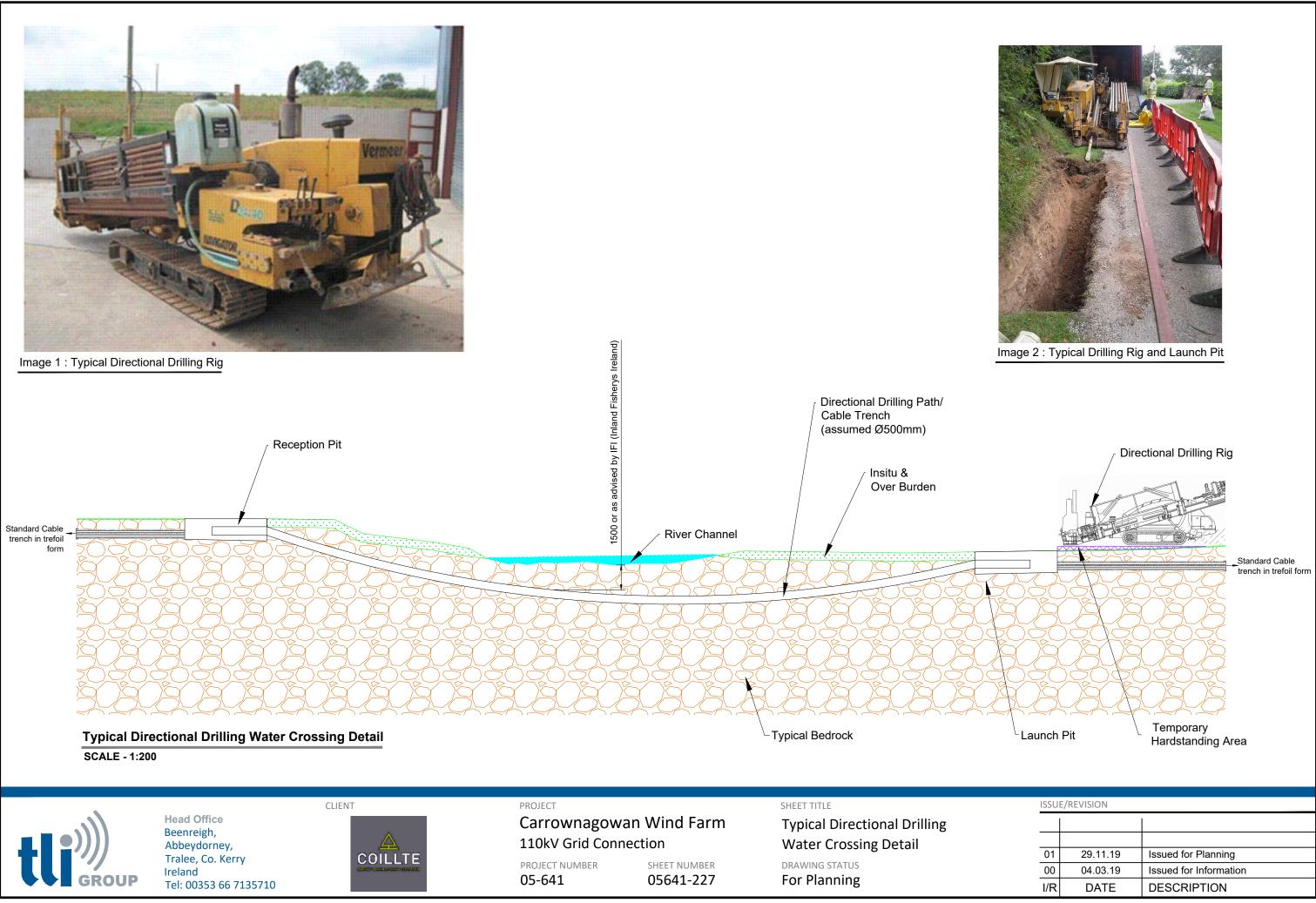
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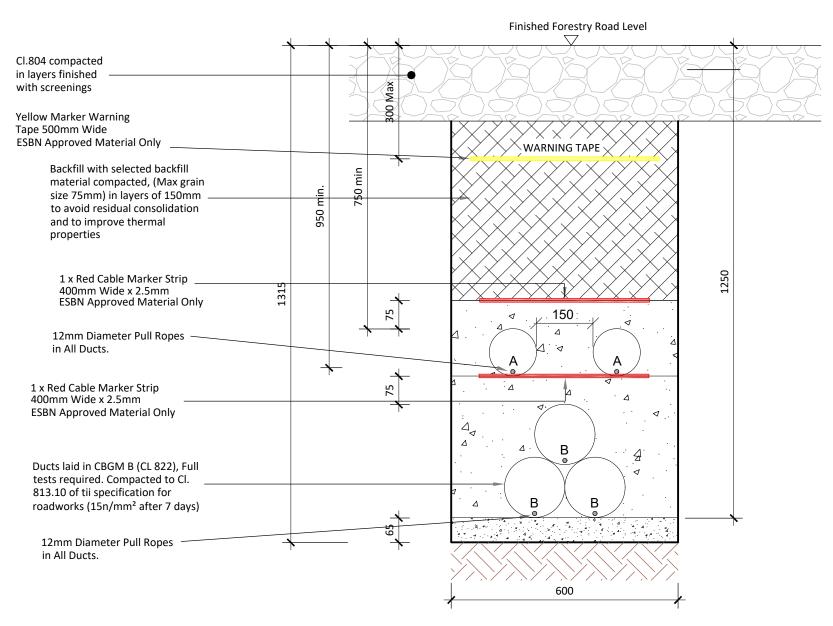
05-641

SHEET TITLE

### Typical Trench Sections for Crossing Watermain/Wastewater

#### SHEET NUMBER





A = 125mm: Outer Diameter HDPE ESB Approved Duct, SDR=17.6 B= 160mm : Outer Diameter HDPE ESB Approved Duct, SDR=21

### **Typical Section Through Forestry Road**

**ALL REINSTATEMENT WORKS ARE TO BE IN** 

**ACCORDANCE WITH LANDOWNERS REQUIREMENTS** 

#### **SCALE 1:10**

#### Note:

- This drawing is to be read in conjunction with • relevant drawings, specifications and reports
- Dimensions are in millimeters, unless noted otherwise
- Drawings are not to be scaled use figured ٠ dimensions only



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Carrownagowan Wind Farm 110 kV Grid Connection PROJECT NUMBER SHEET NUMBER 05-641

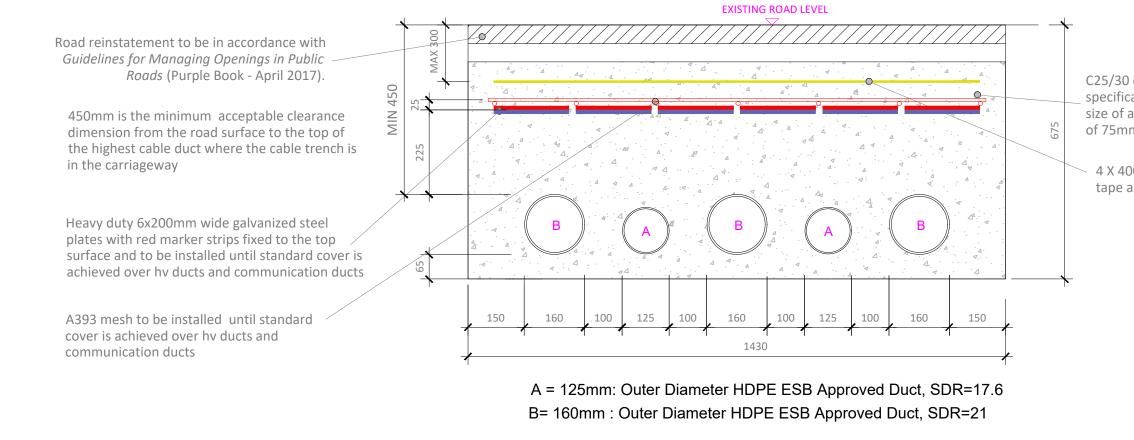
05641-228

SHEET TITLE

Typical Ducting through Forestry Roa - Section and Elevation DRAWING STATUS For Planning

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### **Typical Section Through Ducting in Flat Formation**

ALL REINSTATEMENT WORKS ARE TO BE IN

**ACCORDANCE WITH LOCAL AREA ENGINEERS** 

LANDOWNERS REQUIREMENTS AND GUIDELINES FOR

MANAGING OPENINGS IN PUBLIC ROADS

SHEET NUMBER

05641-229

**SCALE 1:10** 

Note:

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- Dimensions are in millimeters, unless noted otherwise
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F	PROJ	ECT	

Carrownagowan Wind Farm 110 kV Grid Connection

PROJECT NUMBER
05-641

SHEET TITLE

Typical Section Through Ducting in Flat Formation DRAWING STATUS For Planning Checked: SK

C25/30 concrete to be in accordance with specification for road works 1000. 20mm max size of aggregate, with minimum duct spacing of 75mm. Min. cover to steel - 50mm.

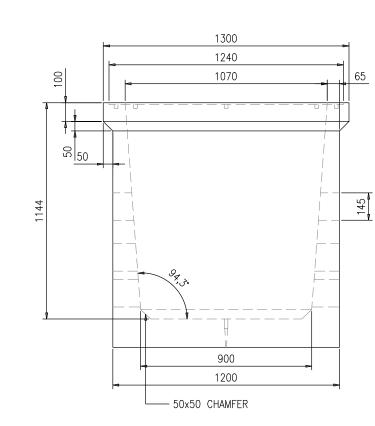
4 X 400mm ESBN yellow warning tape across full width of trench

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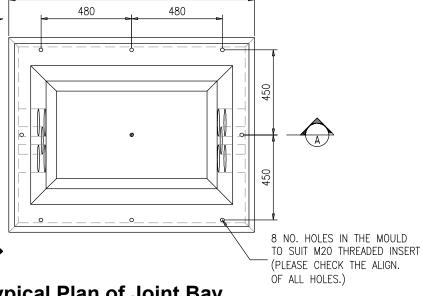
#### NOTES:

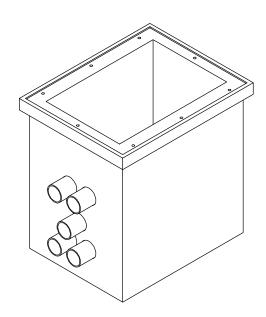
- 1. This drawing is to be read in conjunction with relevant drawings, specifications and reports.
- 2. Dimensions are in millimetres, unless noted otherwise.
- 3. Drawings are not to be scaled use figured dimensions only.
- Reinstatement to comply with requirements of the relevant 4. local Authority/Asset owner
- 5. Entrance & Exit ducts to be in line
- All material and workmanship to be in accordance with the 6. NRA./TII specification for Roadworks, May 2005 and subsequent revisions
- 7. Reinforced concrete to be a minimum grade C32/40, Sulphate resisting cement to be used where aggressive soil conditions apply, refer to table 6.1 of B.S. 8110.
- Carraigeway covers and frames to be to B.S. 124. 8.
- 9. All covers to have ESB logo incorporated in them to the approval of Eirgrid
- 10. Step irons to be hot dipped glvanised to B.S. 729 and positioned as shown on any chamber deeper than 700mm on the end remote from any side entry duct.
- 11. Concrete precast chamber and cover should be tested through a 5 point 40 tonnes vertical static loading test by an independent test company, if required, further details will be provided by Eirgrid.
- 12. Final position of C2 chambers shall be agreed with Eirgrid.
- 13. In a forest environment backfill with lean mix outside the cover frame.



### **C2** Chamber Detail - Section A

**SCALE 1:20** 

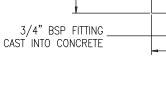




Isometric : C2 Chamber Arrangement



SHEET TITLE PROJECT Carrownagowan Wind Farm **Typical Communications** 110kV Grid Connection Chamber Details PROJECT NUMBER DRAWING STATUS SHEET NUMBER 05-641 05641-230 For Planning



**SCALE 1:20** 

325

294

594

RECESS TO BE 1-2mm

MORE THAT FRAME OF COVER

GRADE C30/37 CONCRETE

TO BE USED AROUND LID

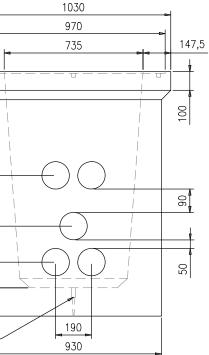
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**Typical Plan of Joint Bay SCALE 1:20** 



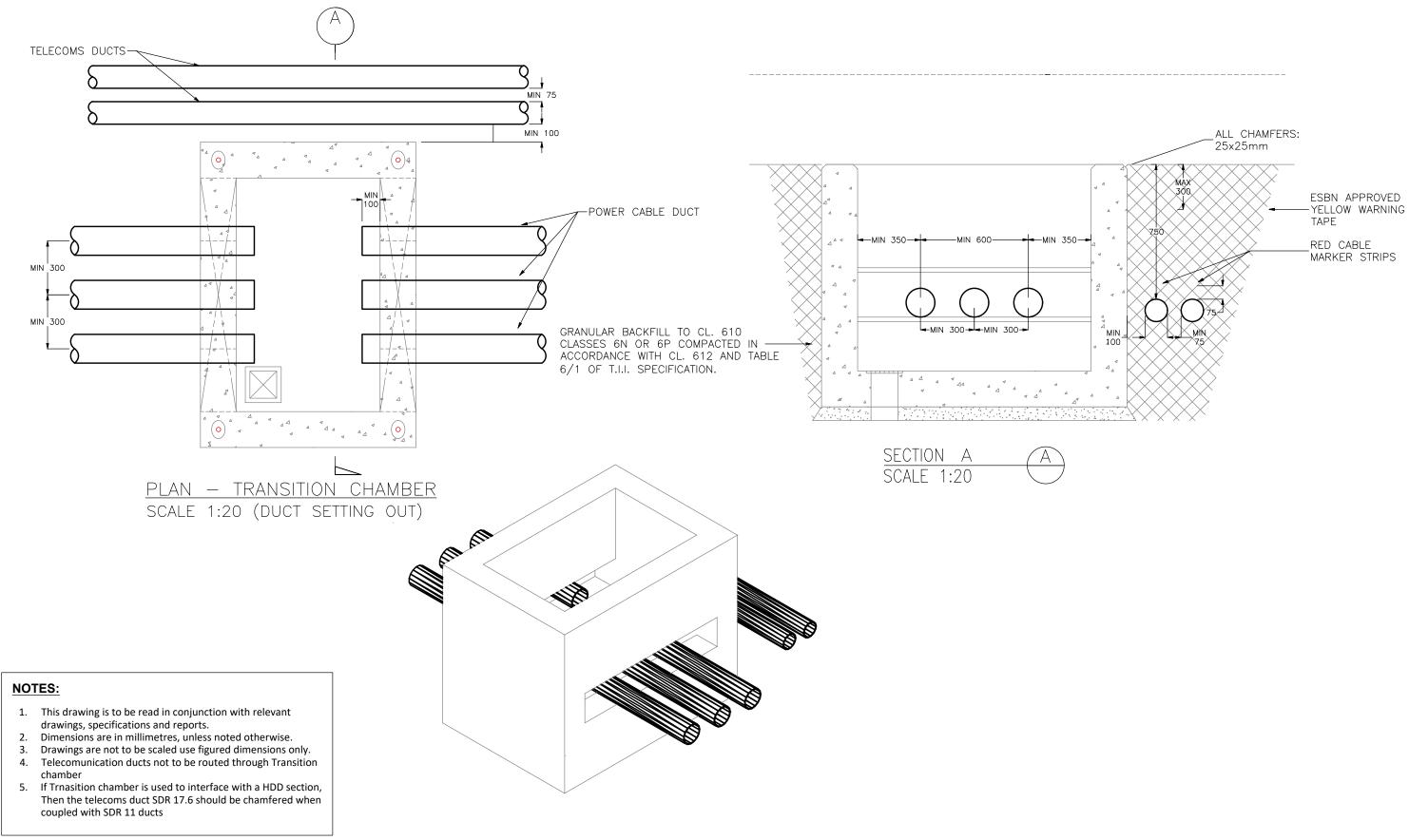
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### **C2** Chamber Detail - Section B

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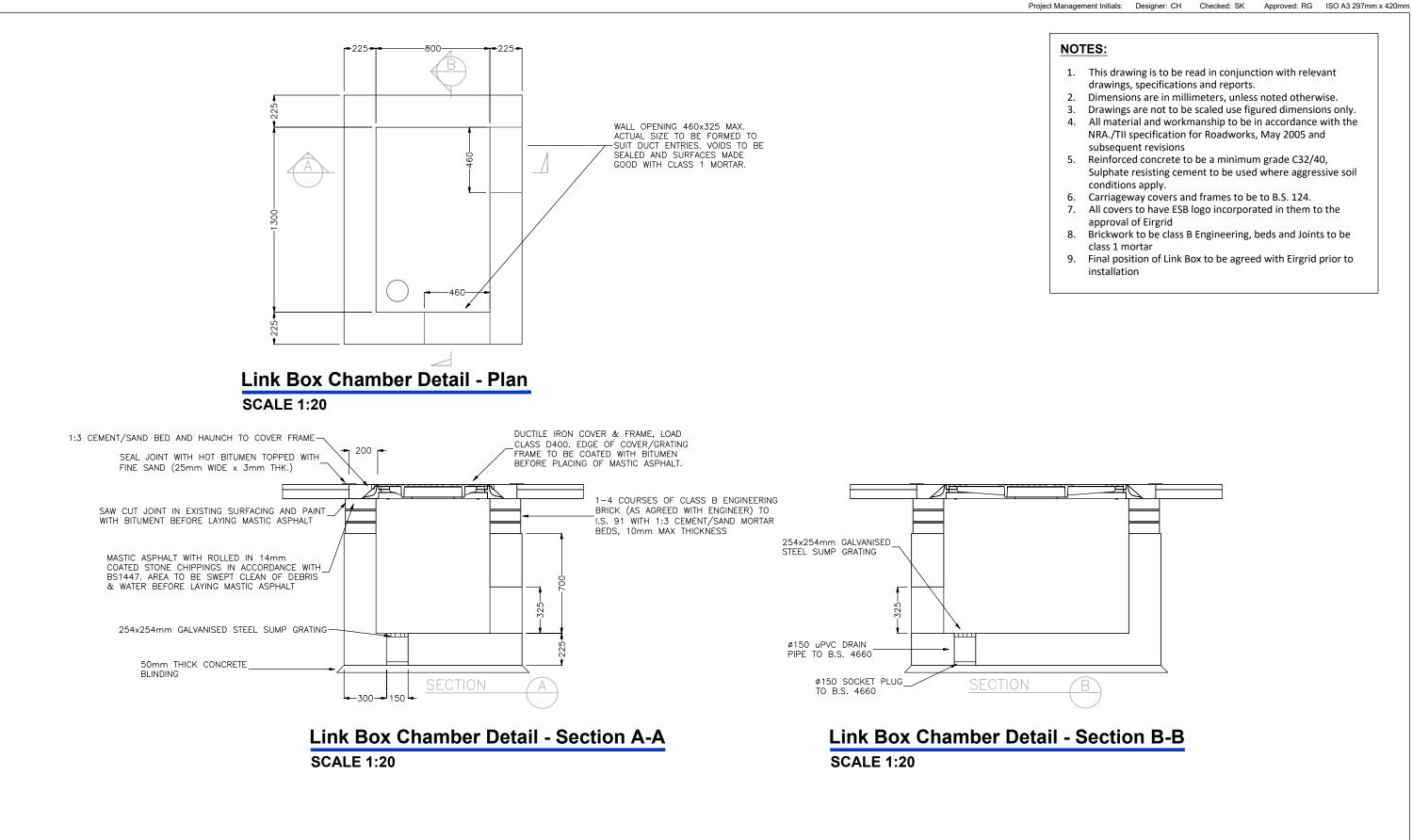
PROJECT	
Carrownagowan Wind Farm	

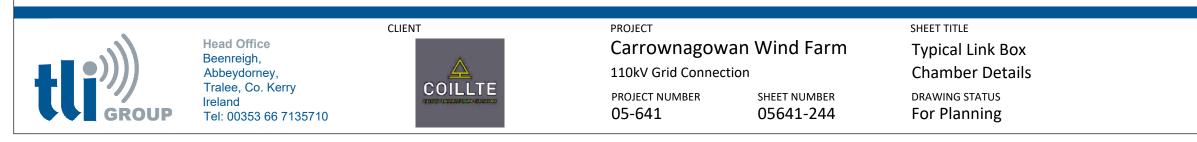
110kV Grid Connection PROJECT NUMBER

SHEET NUMBER 05-641 05641-243 SHEET TITLE

**Typical Transition** Chamber Details DRAWING STATUS For Planning

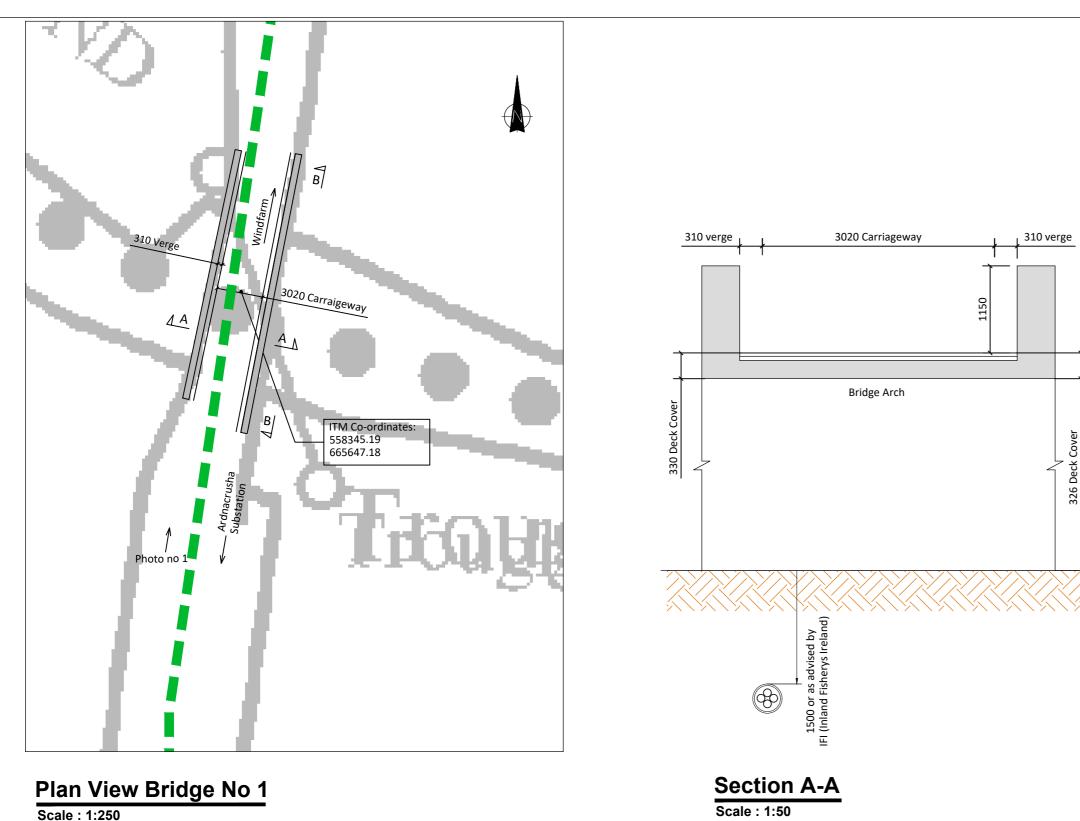
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ISSUE/  00 I/R	/REVISION 18.05.20 DATE	Issued for Planning DESCRIPTION	





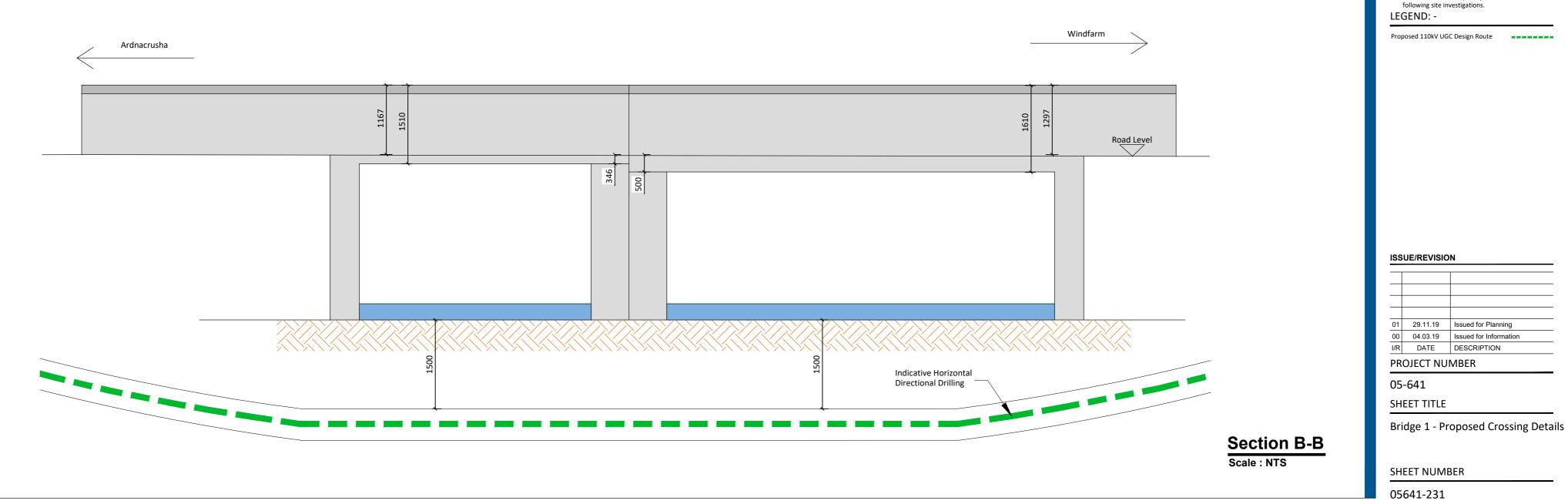
- 1. This drawing is to be read in conjunction with relevant drawings, specifications and reports.
- 2. Dimensions are in millimeters, unless noted otherwise. 3. Drawings are not to be scaled use figured dimensions only. 4. All material and workmanship to be in accordance with the NRA./TII specification for Roadworks, May 2005 and
- 5. Reinforced concrete to be a minimum grade C32/40, Sulphate resisting cement to be used where aggressive soil
- 6. Carriageway covers and frames to be to B.S. 124.
- 7. All covers to have ESB logo incorporated in them to the
- 8. Brickwork to be class B Engineering, beds and Joints to be
- 9. Final position of Link Box to be agreed with Eirgrid prior to

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### Plan View Bridge No 1

Scale : 1:250





### Photo No 1



#### PROJECT

Carrowanagowan Windfarm 110kV Grid Connection

#### CLIENT

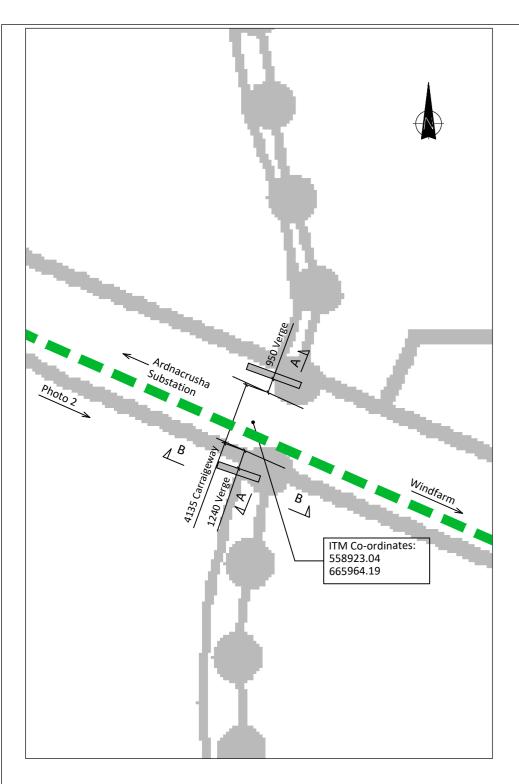


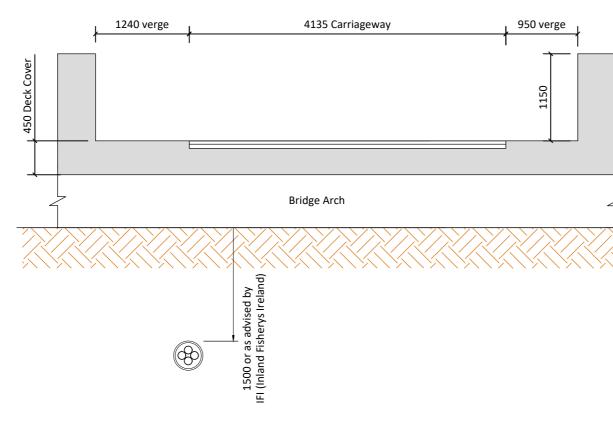
#### CONSULTANTS



#### NOTES: -

- No structural bridge surveys have been carried out and the proposal s are subject to detailed design.
  Bridge crossing designs will be submitted to Clare Co. Council
- bridge dosing early win be submitted to that early early early and the submitted to that early early early and the submitted to that early early early early and the submitted to that early early

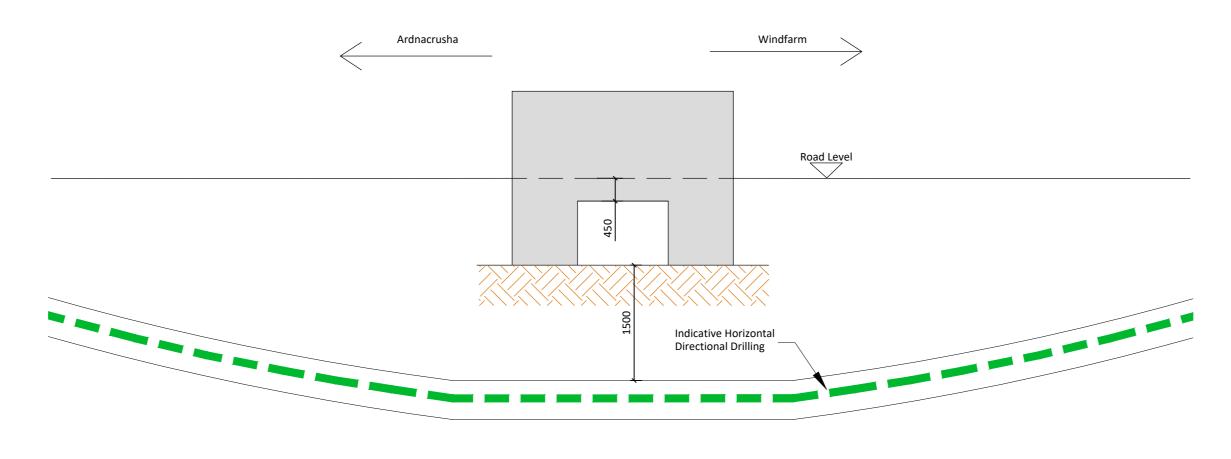




### Plan View Bridge No 2

Scale : 1:250









### Photo No 2



#### PROJECT

Carrowanagowan Windfarm 110kV Grid Connection

#### CLIENT



#### CONSULTANTS



#### NOTES: -

- No structural bridge surveys have been carried out and the proposal s are subject to detailed design.
   Bridge crossing designs will be submitted to Clare Co. Council
- bridge closing designs will be sublitted to clare CC. Council for review.
   Drawings are in compliance with ESBN specification requirements for shallow formation, bridge crossings, etc.
   HDD launch and reception pits locations to be determined following site investigations.

LEGEND: -

Proposed 110kV UGC Design Route

#### ISSUE/REVISION

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00	04.03.19	Issued for Information				
I/R	DATE	DESCRIPTION				
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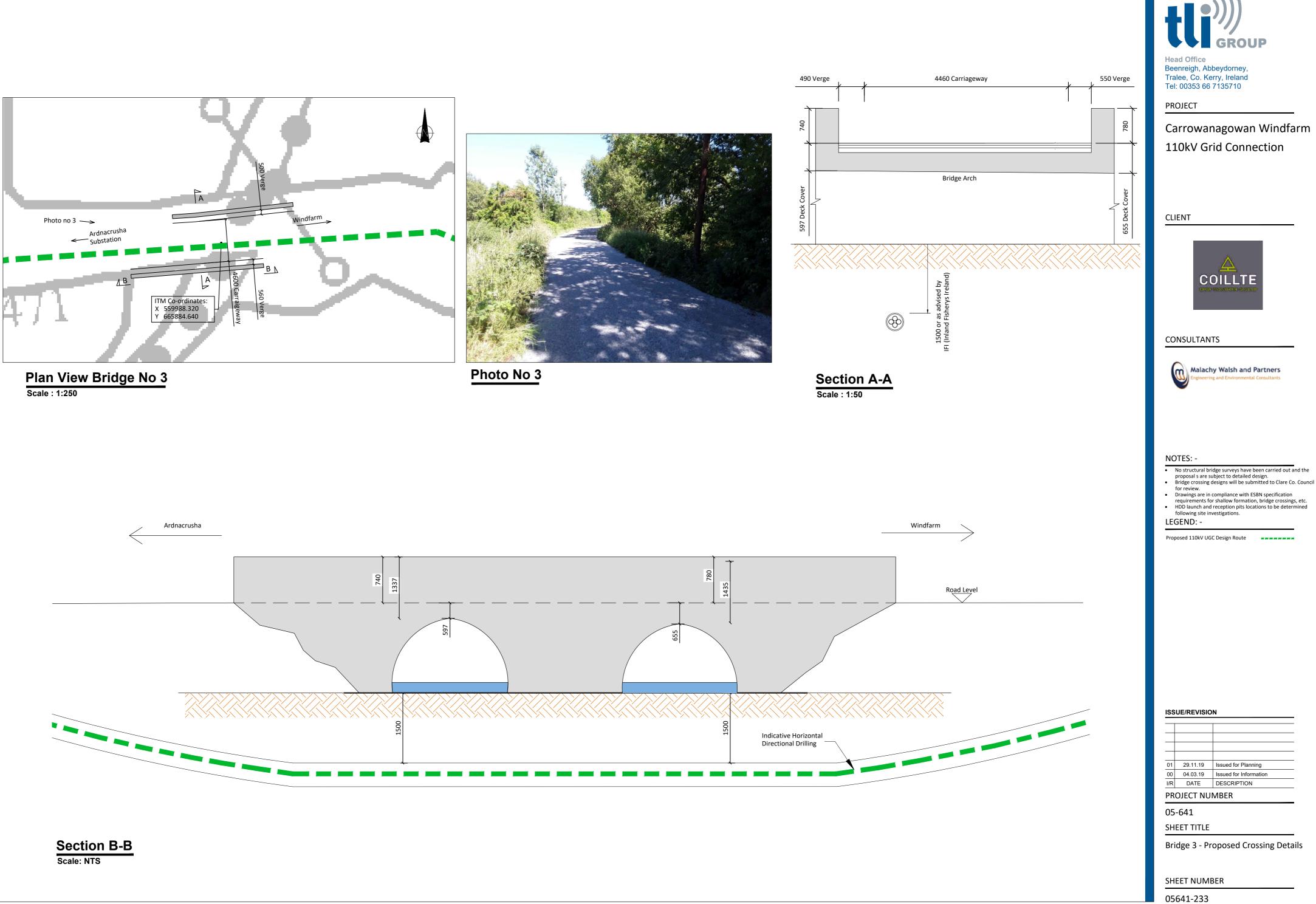
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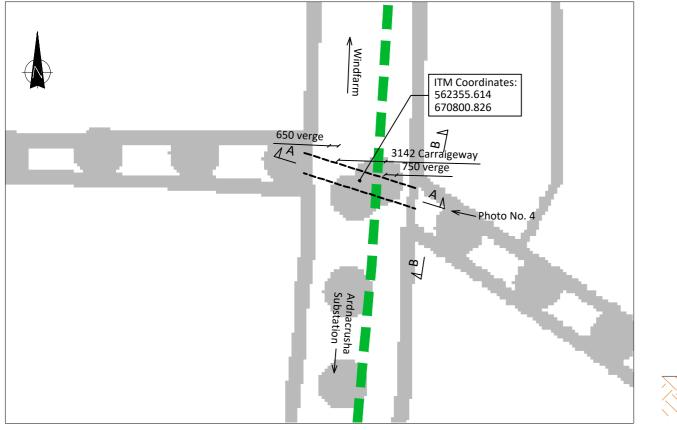
05-641

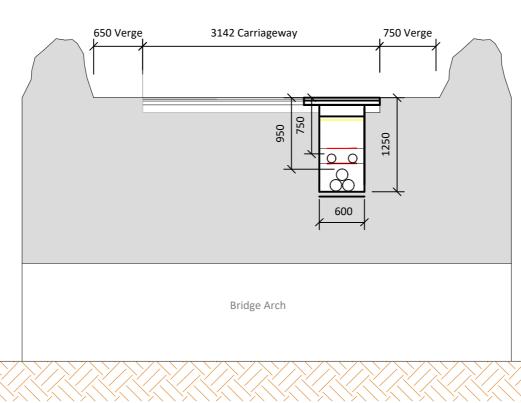
SHEET TITLE

Bridge 2 - Proposed Crossing Details

SHEET NUMBER

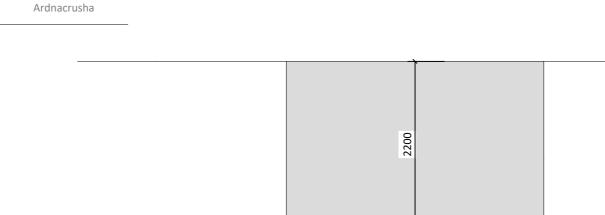






Plan View Bridge No 4 Scale : 1:250





Bridge Arch







Photo No. 4





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PROJECT

Carrowanagowan Windfarm 110kV Grid Connection

#### CLIENT



#### CONSULTANTS



#### NOTES: -

- No structural bridge surveys have been carried out and the proposal s are subject to detailed design.
  Bridge crossing designs will be submitted to Clare Co. Council for provident
- Drawings are in compliance with ESBN specification requirements for shallow formation, bridge crossings, etc.

#### LEGEND:

Proposed 110kV UGC Design Route

#### **ISSUE/REVISION**

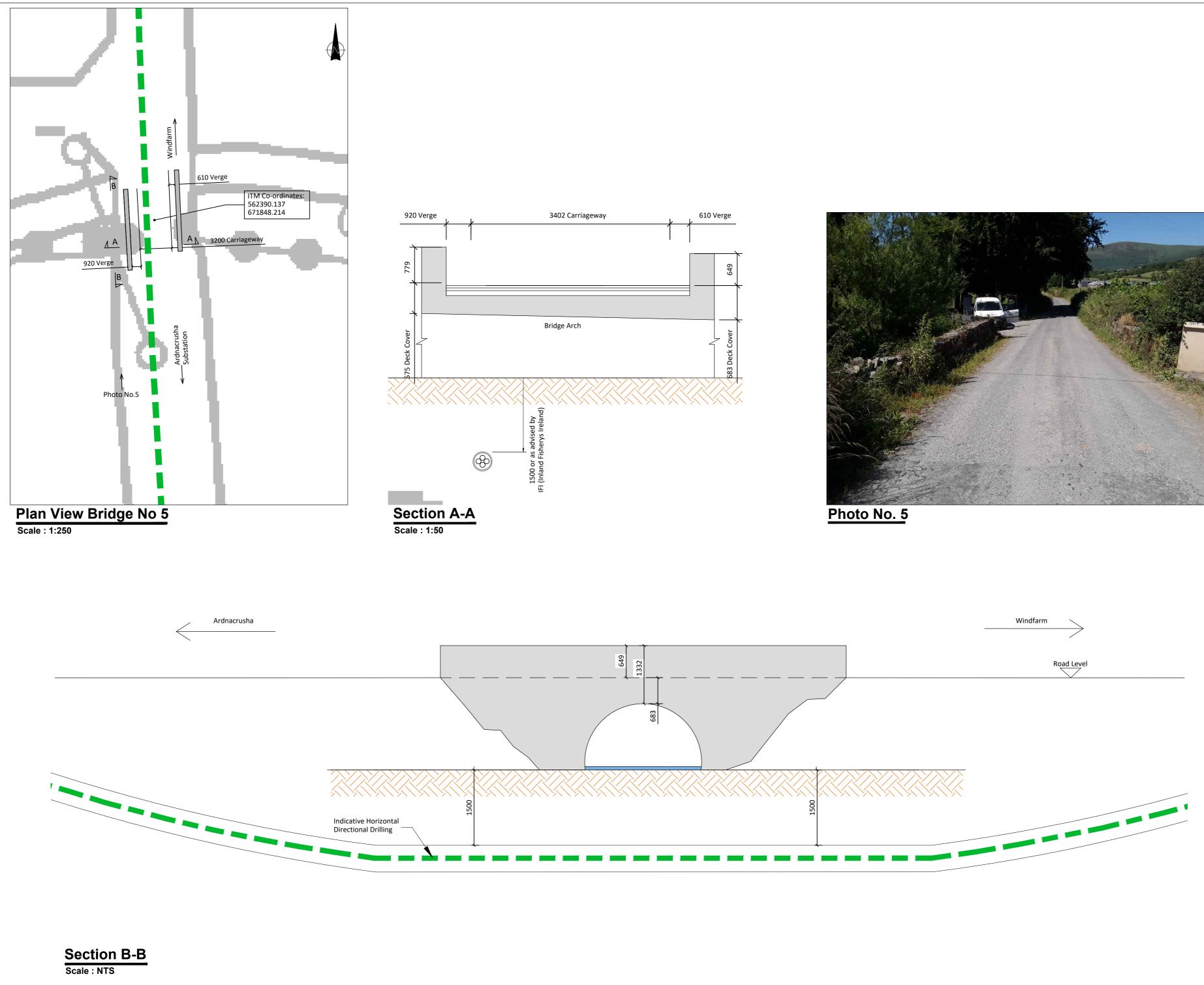
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01	29.11.19	Issued for Planning	
00	04.03.19	Issued for Information	
I/R	DATE	DESCRIPTION	
PROJECT NUMBER			

#### 05-641

SHEET TITLE

Bridge 4 - Proposed Crossing Details

SHEET NUMBER



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#### PROJECT

Carrowanagowan Windfarm 110kV Grid Connection

#### CLIENT



#### CONSULTANTS



#### NOTES: -

- No structural bridge surveys have been carried out and the proposal s are subject to detailed design.
   Bridge crossing designs will be submitted to Clare Co. Council
- bridge dosing early win be submitted to that early early control of a control of the early early of the early early early of the early early
- LEGEND: -

Proposed 110kV UGC Design Route

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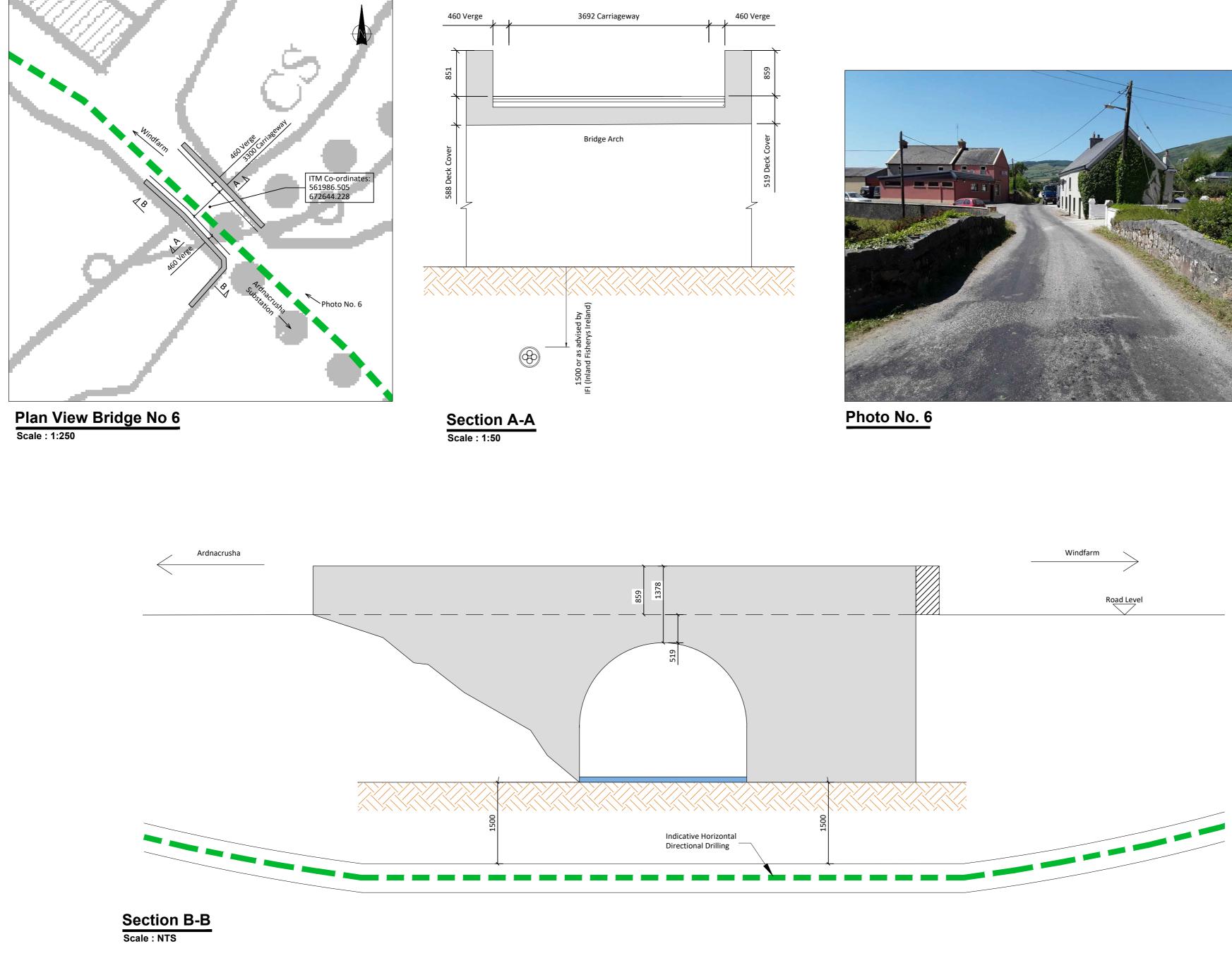
#### PROJECT NUMBER

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SHEET TITLE

Bridge 5 - Proposed Crossing Details

#### SHEET NUMBER



RG





#### PROJECT

Carrowanagowan Windfarm 110kV Grid Connection

#### CLIENT



#### CONSULTANTS



#### NOTES: -

- No structural bridge surveys have been carried out and the proposal s are subject to detailed design.
  Bridge crossing designs will be submitted to Clare Co. Council for review.
  Drawings are in compliance with ESBN specification requirements for shallow formation, bridge crossings, etc.
  HDD launch and reception pits locations to be determined following site investigations.

#### LEGEND: -

Proposed 110kV UGC Design Route

#### ISSUE/REVISION

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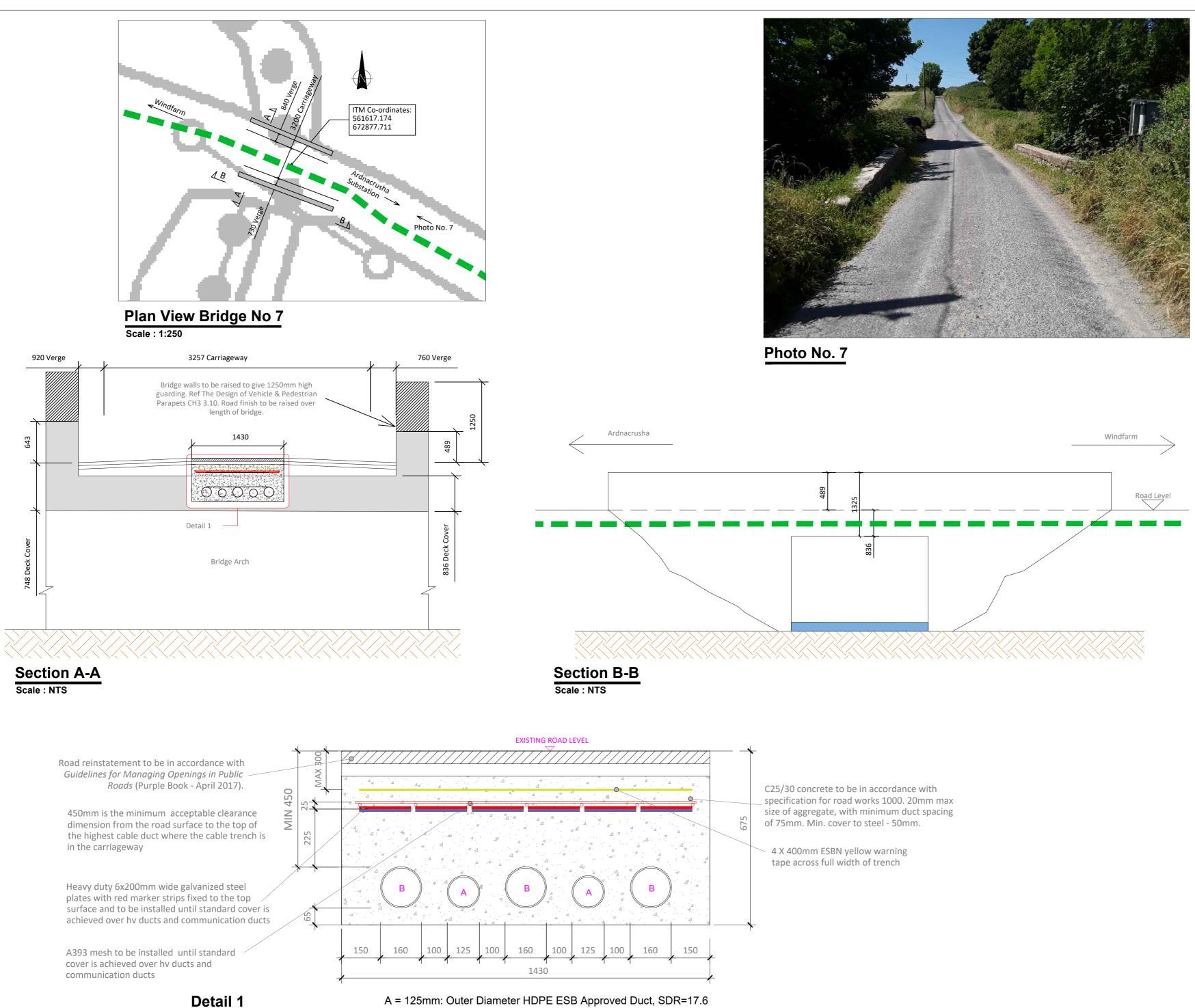
#### PROJECT NUMBER

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SHEET TITLE

Bridge 6 - Proposed Crossing Details

#### SHEET NUMBER



B= 160mm : Outer Diameter HDPE ESB Approved Duct, SDR=21

Scale : 1:10

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#### PROJECT

Carrowanagowan Windfarm 110kV Grid Connection

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#### CONSULTANTS



#### NOTES:

- No structural bridge surveys have been carried out and the proposal s are subject to detailed design.
  Bridge crossing designs will be submitted to Clare Co. Council
- for review.
- Drawings are in compliance with ESBN specification requirements for shallow formation, bridge crossings, etc.

LEGEND:

Proposed 110kV UGC Design Route

#### ISSUE/REVISION

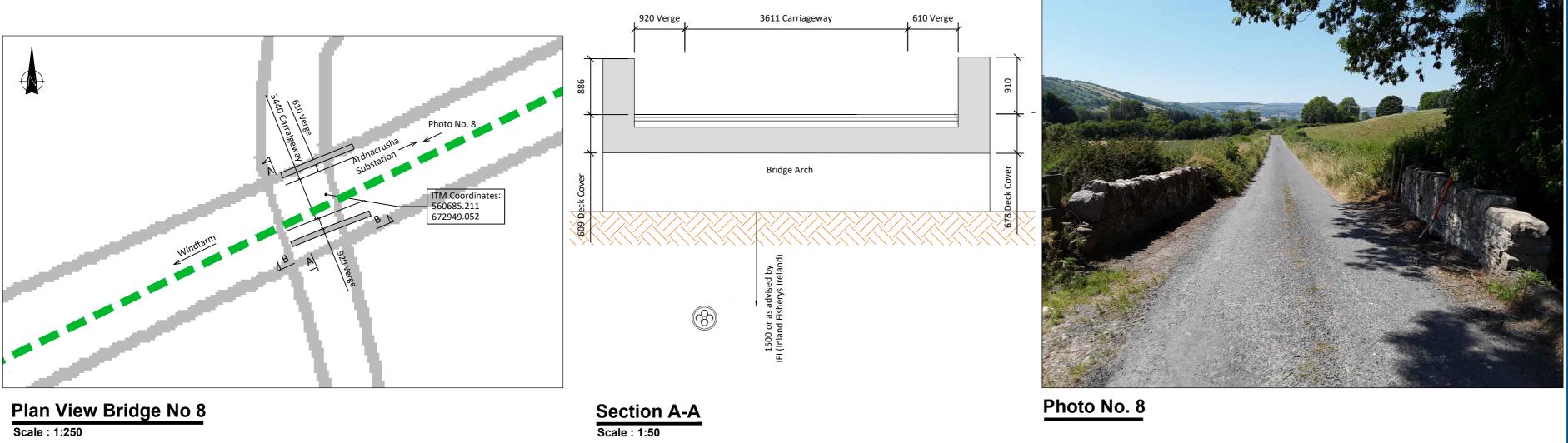
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I/R	DATE	DESCRIPTION	
PROJECT NUMBER			

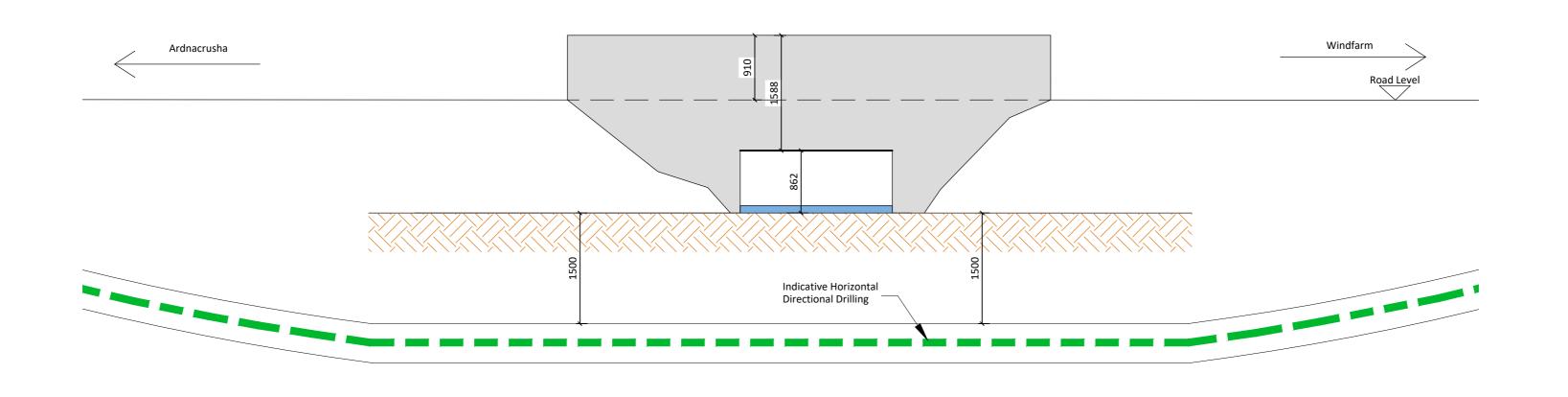
#### 05-641

SHEET TITLE

Bridge 7 - Proposed Crossing Details

SHEET NUMBER









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#### PROJECT

Carrowanagowan Windfarm 110kV Grid Connection

#### CLIENT



#### CONSULTANTS



#### NOTES: -

- No structural bridge surveys have been carried out and the proposal s are subject to detailed design.
  Bridge crossing designs will be submitted to Clare Co. Council
- bridge closing designs will be sublitted to clare CC. Council for review.
   Drawings are in compliance with ESBN specification requirements for shallow formation, bridge crossings, etc.
   HDD launch and reception pits locations to be determined following site investigations.
- LEGEND: -

Proposed 110kV UGC Design Route

#### ISSUE/REVISION

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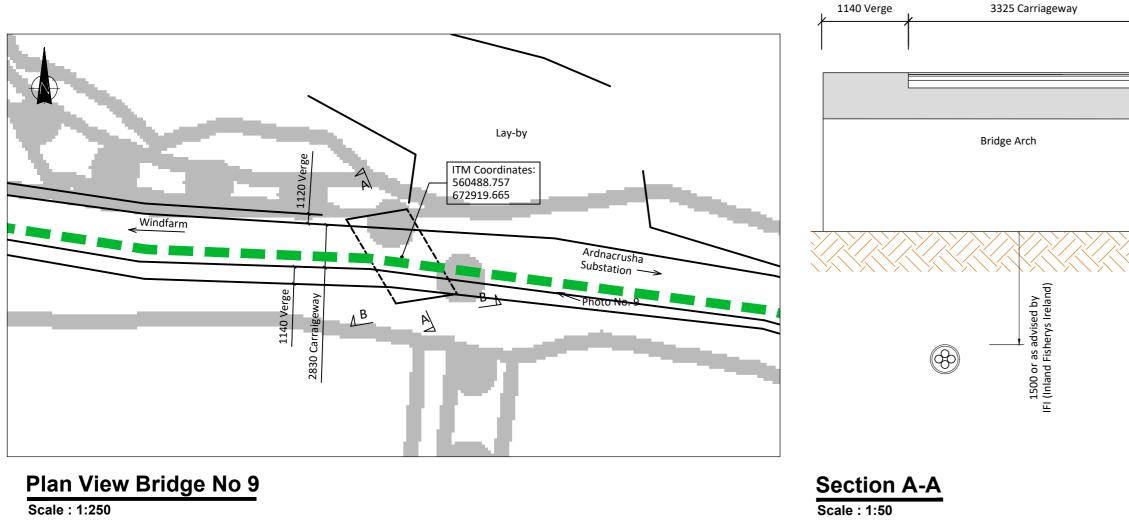
#### PROJECT NUMBER

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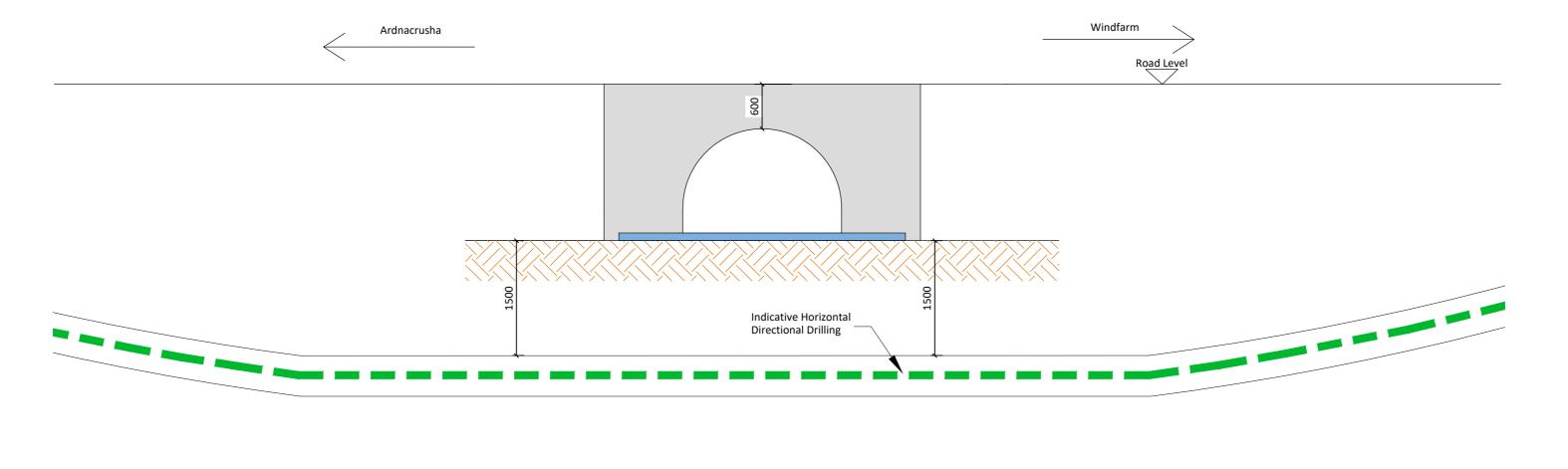
SHEET TITLE

Bridge 8 - Proposed Crossing Details

SHEET NUMBER



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# Scale : 1:50

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RG



### Photo No. 9



#### PROJECT

Carrowanagowan Windfarm 110kV Grid Connection

#### CLIENT



#### CONSULTANTS



#### NOTES: -

- No structural bridge surveys have been carried out and the proposal s are subject to detailed design.
  Bridge crossing designs will be submitted to Clare Co. Council
- bridge closing designs will be sublitted to clare CC. Council for review.
   Drawings are in compliance with ESBN specification requirements for shallow formation, bridge crossings, etc.
   HDD launch and reception pits locations to be determined following site investigations.
- LEGEND: -

Proposed 110kV UGC Design Route

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00	04.03.19	Issued for Information			
I/R	DATE	DESCRIPTION			
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#### PROJECT NUMBER

05-641

SHEET TITLE

Bridge 9 - Proposed Crossing Details

#### SHEET NUMBER

			Culvert Crossing Schedule		
Culvert No.	Dimensions (mm)	Material	Approx. Cover (mm)	Proposed Crossing Methodology	Photo
1.	350 Ø	Concrete	900	UNDERCROSSING	
2.	300 Ø	HDPE	200	UNDERCROSSING	
3.	2x600 Ø	Concrete	1800	OVERCROSSING	
4.	600 wide x 800 deep	Stone	1000	UNDERCROSSING	
5.	600 Ø	HDPE	200	UNDERCROSSING	
6.	250 Ø	Concrete	500	UNDERCROSSING	
7.	600 Ø	Concrete	700	UNDERCROSSING	
8.	400 wide x 500 deep	Stone	900	UNDERCROSSING	
9.	600 wide x 500 deep	Stone	900	UNDERCROSSING	



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01	29.11.19	Issued for Planning		
00	04.03.19	Issued for Information		
I/R	DATE	DESCRIPTION		

#### PROJECT NUMBER

05-641

SHEET TITLE

Proposed Culvert Crossings Sheet 1 of 3

SHEET NUMBER

			Culvert Crossing Schedule		
Culvert No.	Dimensions (mm)	Material	Approx. Cover (mm)	Proposed Crossing Methodology	Photo
10.	600 Ø	HDPE	500	UNDERCROSSING	
11.	300 Ø	HDPE	600	UNDERCROSSING	
12.	2x750 Ø	HDPE	2000	OVERCROSSING	
15.	300 Ø 375 Ø	HDPE HDPE	600 700	UNDERCROSSING	
16.	375 Ø	HDPE	700	UNDERCROSSING	
17.	375 Ø	HDPE	650	UNDERCROSSING	
18.	375 Ø	HDPE	350	UNDERCROSSING	
19.	600 Ø	HDPE	800	UNDERCROSSING	

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Carrowanagowan Windfarm
110kV Grid Connection
CLIENT
Malachy Walsh and Partners Engineering and Environmental Consultants
NOTES: -
<ul> <li>No structural surveys have been carried out and the proposals are subject to detailed design.</li> <li>Crossings are in compliance with ESBN &amp; Eirgrid specification requirements for shallow formation, min depth, etc.</li> <li>Additional culverts may be encountered on the route.</li> </ul>
LEGEND: -

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### PROJECT NUMBER

05-641

SHEET TITLE

Proposed Culvert Crossings Sheet 2 of 3

SHEET NUMBER

Culvert Crossing Schedule						
Culvert No.	Dimensions (mm)	Material	Approx. Cover (mm)	Proposed Crossing Methodology	Photo	
22.	600 Ø	Concrete	550	UNDERCROSSING		
23.	300 Ø	Concrete	600	UNDERCROSSING		
24.	250 Ø	HDPE	100	UNDERCROSSING		
25.		NEW CONCRETE ARCH CULVERT TO BE INSTALLED OVER RIVER		OVERCROSSING		
26.	450 Ø	CONCRETE	1000	UNDERCROSSING		
27.	300 Ø	CONCRETE	750	UNDERCROSSING		
28.	900 (Width per span)	Two Span Masonry	700	UNDERCROSSING		



#### PROJECT

Carrowanagowan Windfarm 110kV Grid Connection

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#### NOTES: -

- No structural surveys have been carried out and the proposals are subject to detailed design.
  Crossings are in compliance with ESBN & Eirgrid specification requirements for shallow formation, min depth, etc.
  Additional culverts may be encountered on the route.

LEGEND: -

#### ISSUE/REVISION

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I/R	DATE	DESCRIPTION
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#### PROJECT NUMBER

05-641

SHEET TITLE

Proposed Culvert Crossings Sheet 3 of 3

SHEET NUMBER



Project: Carrownagowar	WF – 110kV Grid Connection	Ref: rev0
Section: 110kV UGC Ra	ting Check	Job No: 05-641
		Date: 04/03/2019
Made By: DB	Checked By: SK	Sheet No: 1 of 7

#### Instruction:

Technical Lead: Ruairi Geary (TLI Group)

#### Date of Writing: 04/03/2019

Scope of Note: Summary of cable rating check carried out for the 110kV grid connection cable

Documents & Data Issued for Review: N/A

#### **Details:**

TLI Group (the Consultant) were engaged by Coillte (the Client) working with Malachy Walsh and Partners to identify and design the 110kV grid connection for Carrownagowan Windfarm as part of the planning application process. The 110kV grid connection for Carrownagowan Windfarm will be rated for a maximum export capacity (MEC) of 90MW to the relevant transmission interface identified by the TSO as appropriate. Both overhead line and underground cable options were identified to Ardnacrusha and Ennis Substations, however the Client decided to progress an underground cable option from the prospective Carrownagowan Windfarm site location with the associated grid connection via Ardnacrusha substation.

A cable rating study was carried out to check the suitability of various 110kV cable sizes/types for the project's MEC and the current cable route design. The purpose of this exercise was to check the load capacity of each cable for the typical trench designs incorporated as part of the cable route design under max load conditions.

The following 110kV cable types/sizes were examined as part of this cable rating check:

- NKT 1600mm.sq Al Cable
- NKT 1000mm.sq Al Cable

Cable Study Parameters				
Nominal Voltage:	110kV			
Power:	90MW			
Power Factor:	0.95			
Cable Length:	750m (avg. section length)			
Cable Trench Design:	See Appendix A, B, C			
Ambient Temp (Soil)	20°C (Summer rating)			
Soil Thermal Resistivity	1.2 K·m/W (Summer rating)			
Backfill Thermal Resistivity	1 K·m/W (Summer rating)			



an WF – 110kV Grid Connection	Ref: rev0
ating Check	Job No: 05-641
	Date: 04/03/2019
Checked By: SK	Sheet No: 2 of 7
	an WF – 110kV Grid Connection ating Check Checked By: SK

#### **Cable Study Results**

#### Trefoil Trench Design:

The cable study analysis found that installing an **NKT 1600mm<sup>2</sup> AL XLPE (110kV) UGC** over a distance of 750m using the standard trefoil trench design detailed in Appendix A, with the UGC in a Trefoil arrangement, a loading of 49% (Figure 1) on the UGC is well within the maximum design loading capacity of 90% which would generally be utilized. From this analysis a **loading capacity of 49%** offers the potential of extending this loading factor further up to a maximum design capacity of 90% and would indicate that there is sufficient capacity for load growth on the site.

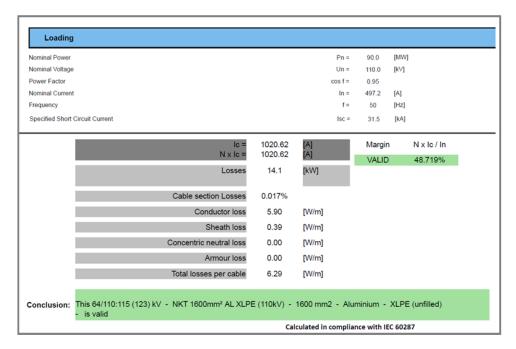


Figure 1 Cable Study Results - 1600mm.sq Al

For comparison reasoning, an alternative cable study was generated incorporating an **NKT 1000mm<sup>2</sup> AL XLPE** (110kV) UGC again over a distance of 750m, installed within a Trefoil arrangement as per the trench detail in Appendix A and supplying a load of 90MW. It was found as a result that the cable being loaded to approximately 59% of its maximum loading capacity (Figure 2). From these studies it can be concluded that either cable size would offer favourable potential loading capacity for Carrownagowan Windfarm under full load operating conditions



Project:	roject: Carrownagowan WF – 110kV Grid Connection Re				Ref: rev0		
Section:	110kV UGC Rating Ch	ieck		Job No:	05-641		
				Date:	04/03/2019		
Made By:	DB	Checked By:	SK	Sheet No:	3 of 7		

Nominal Power		Pn =	90.0	[MW]	
Nominal Voltage		Un =	110.0	[kV]	
Power Factor		cos f =	0.95		
Nominal Current		In =	497.2	[A]	
Frequency		f =	50	[Hz]	
Specified Short Circuit Current		Isc =	31.5	[kA]	
ic N x ic	= 846.47 = 846.47	[A] [A]	Margir	ו	N x lc / ln
			VALIE	)	58.742%
Loss	es 20.0	[kW]			
Cable section Loss	es 0.023%				
Conductor lo	ss 8.55	[W/m]			
Sheath lo	ss 0.30	[W/m]			
Concentric neutral lo	ss 0.00	[W/m]			
Armour lo	ss 0.00	[W/m]			
	le 8.86	[W/m]			

Figure 2 Cable Study Results - 1000mm.sq Al

#### Flat Formation Trench Design:

The cable study analysis also incorporated the alternative cable trench design in a Flat Formation arrangement again using **NKT 1600mm<sup>2</sup> AL XLPE (110kV) UGC** with consideration to a depth level of 600mm as per the centre of duct with reference to the trench design detailed in Appendix B. With the UGC installed in a Flat Formation arrangement, supplying a load of 90MW, the result representation shows cable being loaded to approximately **48% of its maximum loading capacity** (Figure 3).

Nominal Power		Pn =	90.0	[MW]	
Nominal Voltage		Un =	110.0	[kV]	
Power Factor		cos f =	0.95		
Nominal Current		In =	497.2	[A]	
Frequency		f =	50	[Hz]	
Ic =	1049.88	[A]	Margi	n	N x lc / In
N x lc =	1049.88	[A]	VALIE	)	47.361%
Losses	16.1	[kW]			
Cable section Losses	0.021%				
Conductor loss	6.10	[W/m]			
Sheath loss	1.04	[W/m]			
Concentric neutral loss	0.00	[W/m]			
Armour loss	0.00	[W/m]			
Total losses per cable	7.15	[W/m]			

Figure 3 Flat formation cable study results - 1600mm.sq AL



Project: Carrownagowan WF -	- 110kV Grid Connection	Ref: rev0
Section: 110kV UGC Rating C	heck	Job No: 05-641
		Date: 04/03/2019
Made By: DB	Checked By: SK	Sheet No: 4 of 7

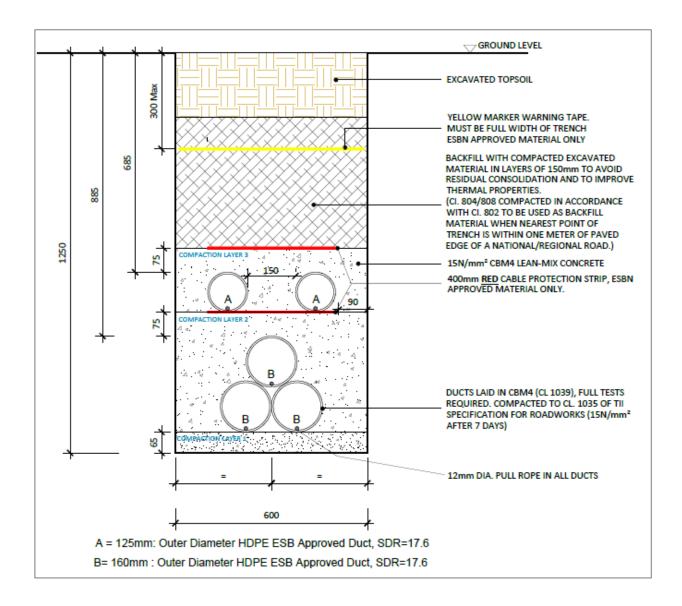
#### Horizontal Directional Drilling Trench Design:

Another interpretation of the UGC installation is (HDD) method as per Appendix C, which consists of the potential crossing of (e.g. Bridge, watercourses etc.) that the cable may encounter. The study was carried out to illustrate this installation method again with **NKT 1600mm<sup>2</sup> AL XLPE (110kV) UGC** with consideration to a depth level of circa. 4000mm, ducts directly buried within native soil surround to comprehend the worst possible case scenario. The arrangement was installed as a trefoil, suppling a full load again of 90MW, the result would be that the UGC being loaded to approximately **55.4% of its maximum loading capacity** (Figure 4) under operating conditions.

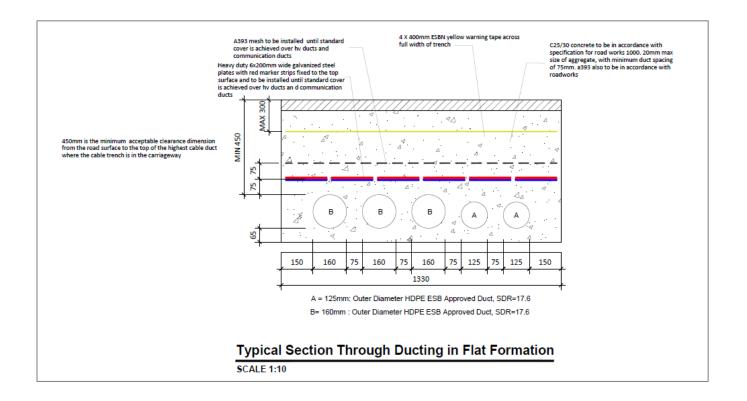
Iominal Power			Pn	= 90.0	[MW]	
Iominal Voltage			Un	= 110.0	[kV]	
ower Factor			cos f	= 0.95		
Nominal Current			In	= 497.2	[A]	
requency			f	= 50	[Hz]	
	lc =	897.84	[A]	Margir	1	N x lc / ln
	N × Ic =	897.84	[A]	VALID	1	55.382%
	Losses	11.5	[kW]			
	Cable section Losses	0.014%				
	Conductor loss	5.98	[W/m]			
	Sheath loss	0.39	[W/m]			
	Concentric neutral loss	0.00	[W/m]			
	Armour loss	0.00	[W/m]			
	Total losses per cable	6.37	[W/m]			

Figure 4 HDD Trefoil cable arrangement study results - 1600mm.sq AL

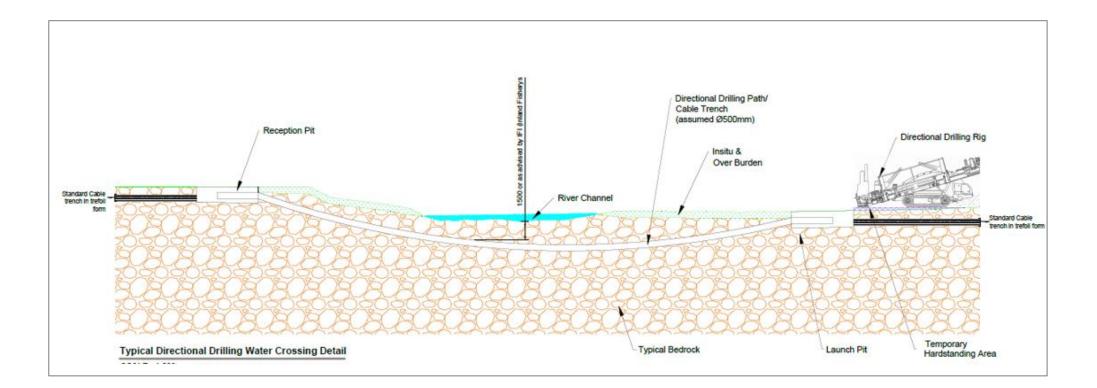
### **Appendix A – Standard Trefoil Trench Design**



### **Appendix B – Flat Formation Trench Design**



### **Appendix C – Horizontal Directional Drill Trench Design**





Project: Carrownagowan	VF – 110kV Grid Connection	Ref:	Rev2
Section: UG Cable Pulling	Calculation Check	Job No:	05-641
		Date:	04/02/2020
Made By: DB	Checked By: SK	Sheet No:	1 of 7

#### Instruction:

Technical Lead: Ruairi Geary (TLI Group)

Date of Writing: 04.02.20 (rev2)

Scope of Note: Summary of cable pulling calculations check on sections of the UGC route.

Documents & Data Issued for Review: N/A

#### **Details:**

TLI Group (the Consultant) were engaged by Coillte (the Client) working with Malachy Walsh and Partners to identify and evaluate Cable Pulling Calculations from 110kV Ardnacrusha Substation to Carrownagowan Windfarm for the proposed 110kV grid connection as part of the planning application process. The purpose of this Technical Note is to outline the calculations completed to ensure that the maximum pulling tension and side wall bearing pressure limits of the installed cable would not be exceeded during construction. These calculations were based on the current design, elevations and profile details for the UGC route recorded as part of the topographical survey which was carried out for the entire UGC route.

For the cable pulling calculations check it has been assumed that an NKT 1600mm.sq Al Cable is to be installed as part of this project. The following pulling tension and side wall bearing pressure limits apply to this cable and have been used as part of the calculations:

Cable Type:	NKT 1600mm <sup>2</sup> AL XLPE (110kV)
Max Pulling Tension	4894.56 kg (force)
Max Side Wall Bearing Pressure:	1019.7 kg/m (force) for Cables installed within ducts

These limits have been formulated, originating from **Item 16** and **Item 17** as per the cable functional specifications (See Appendix A) deriving from kilo-newton meter (kN/m) measurement units to kilogram meter unit for calculation purposes applying the following a conversion rate:

#### $1kN/m \approx 101.97 kg/m$



Project: Carrownagowan WF	- 110kV Grid Connection	Ref:	Rev2
Section: UG Cable Pulling Cal	culation Check	Job No:	05-641
		Date:	04/02/2020
Made By: DB	Checked By: SK	Sheet No:	2 of 7

#### Section 1 – JB07-JB08

On review of the pinch point section highlighted within JB07-JB08. The cable pulling study analysis found that installing an **NKT 1600mm<sup>2</sup> AL XLPE (110kV) UGC** from either side would result in approximate pulling tension values of **896.23kg** and **1590.5kg** respectively in keeping with the manufactures specified limit of 4894.56kg

The cable pulling study also found consistent values for the maximum permissible sidewall force allowable with approx. **170.7kg/m** when installed from JB07 and approx. **53.18kg/m** when installed from JB08. This ensures that the maximum pulling tension and side wall bearing pressure limits of the cable to be installed would not be exceeded during construction based on the current design

SECTIO	N DETAILS														
CIRCUIT	Ardnacrusha - Carrownagowan														
ROUTE SECTION	1														
CABLE SECTION	JB07-JB08														
FROM	JB07														
TO	JB08														
CALCULATIO	N PARAMETERS	1													
CABLE WEIGHT (kg/m)	9.7														
C.O.F. (DUCT)	0.2														
PULL TYPE	NOSE PULL														
			STRA	IGHT		BEND					CALCULATION				
			31104			DEND			JB07	TO	JB08	JB08	TO	JB07	
SEGMENT NO.	SEGMENT TYPE	DUCTED/DIR ECT BURIAL	LENGTH	SLOPE	BEND ANGLE	RADIUS	ARC LENGTH	COF	NOSE TENSION	SWP	CHAINAGE	NOSE TENSION	SWP	CHAINAGE	REMARKS
			m	deg	deg	т	m		kg	kg/m	m	kg	kg/m	m	
0	ENTRY/EXIT TENSION								0	0	0	1590.5	53.18		
1	STRAIGHT PULL	DUCTED	14.7	0.0				0.2	28.5		14.7	1590.5		687.9	
2	HORIZONTAL BEND	DUCTED			17.0	29.4	8.7	0.2	45.5	1.55	23.4	1562.0	53.18	673.2	
3	STRAIGHT PULL	DUCTED	181.2	0.0			0.0	0.2	397.0		204.6	1470.5	-	664.5	BRIDGE 1 CROSSING
4	HORIZONTAL BEND	DUCTED			5.0	121.6	10.6	0.2	418.8	3.44	215.2	1119.0	9.20	483.3	
5	STRAIGHT PULL	DUCTED	97.5	2.0			0.0	0.2	640.8		312.7	1090.8	-	472.7	
6	HORIZONTAL BEND	DUCTED			6.0	44.8	4.7	0.2	657.1	14.68	317.3	868.8	19.41	375.2	
7	STRAIGHT PULL	DUCTED	222.1	4.0			0.0	0.2	1237.2	-	539.4	848.7	-	370.5	
6	HORIZONTAL BEND	DUCTED			92.0	10.0	16.1	0.2	1706.9	170.69	555.5	268.6	26.86	148.5	
7	STRAIGHT PULL	DUCTED	132.4	-3.0			0.0	0.2	1896.2	-	687.9	189.3	-	132.4	
	ENTRY/EXIT TENSION								1896.23	170.69		0	0	0	1

Figure 1 Cable Pulling Calculation – JB07-JB08



Project: Carrownagowan WF	- 110kV Grid Connection	Ref: Rev2	2
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#### Section 2 – JB11-JB12

On review of the pinch point section highlighted within JB11-JB12. The cable pulling study analysis found that installing an **NKT 1600mm<sup>2</sup> AL XLPE (110kV) UGC** from either the Entry pit or Exit pit would result in approximate pulling tension values of **2727kg** and **2178.9kg** respectively in keeping with the manufactures specified limit of 4894.56kg

The cable pulling study also found consistent values for the maximum permissible sidewall force allowable with approx. **218.76kg/m** when installed from JB11 and approx. **70.28kg/m** when installed from JB12. This ensures that the maximum pulling tension and side wall bearing pressure limits of the cable to be installed would not be exceeded during construction based on the current design.

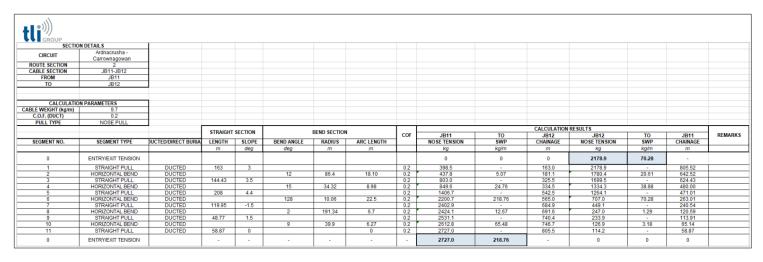


Figure 2 Cable Pulling Calculation - JB11-JB12



Project: Carrownagowan WF	<ul> <li>– 110kV Grid Connection</li> </ul>	Ref:	Rev2
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Section 4 – (JB24-JB25, JB25-JB26, JB27-JB28)

On review of the pinch point section highlighted within JB24-JB25. The cable pulling study analysis found that installing an **NKT 1600mm<sup>2</sup> AL XLPE (110kV) UGC** from either side would result in approximate pulling tension values of **2928.93kg** and **998.43kg** respectively in keeping with the manufactures specified limit of 4894.56kg

The cable pulling study also found consistent values for the maximum permissible sidewall force allowable with approx. **367.06kg/m** when installed from JB24 and approx. **54.19kg/m** when installed from JB25. This ensures that the maximum pulling tension and side wall bearing pressure limits of the cable to be installed would not be exceeded during construction based on the current design.

SECTION D	ETAILS														
CIRCUIT	Ardnacrusha - Carrownagowan														
ROUTE SECTION	4														
CABLE SECTION	JB24-JB25														
FROM	JB24														
TO	JB25														
CALCULATION P															
	9,7														
CABLE WEIGHT (kg/m) C.O.F. (DUCT)	9.7														
PULL TYPE	NOSE PULL														
FULL TIFE	NOSE FOLL							-				ON RESULTS			
			STRAIGHT	SECTION		BEND SECTION	4		JB24	TO	JB25	JB25	TO	JB24	-
SEGMENT NO.	SEGMENT TYPE	DUCTED/DIRECT BURIAL	LENGTH	SLOPE	BEND ANGLE	RADIUS	ARC LENGTH	COF	NOSE TENSION	SWP	CHAINAGE	NOSE TENSION	SWP	CHAINAGE	REMAR
		DOMAL	m	deg	deg	m	m		kg	kg/m	m	kg	kg/m	m	
0	ENTRY/EXIT TENSION								0	0	0	998.43	54.19	-	
1	STRAIGHT PULL	DUCTED	53.00					0.20	102.82	-	53.00	998.43	-	693.03	-
2	HORIZONTAL BEND	DUCTED			23.00	243.25	97.65	0.20	292.97	1.20	150.65	895.61	3.68	640.03	
3	STRAIGHT PULL	DUCTED	66.00					0.20	421.01	-	216.65	695.65	-	542.39	
4	HORIZONTAL BEND	DUCTED			18.00	131.33	41.26	0.20	506.20	3.85	257.91	567.61	4.32	476.39	
5	STRAIGHT PULL	DUCTED	28.77					0.20	562.01	-	286.68	481.05	-	435.13	
6	HORIZONTAL BEND	DUCTED			22.00	93.57	35.93	0.20	645.73	6.90	322.60	425.24	4.54	406.36	
7	STRAIGHT PULL	DUCTED	20.00					0.20	684.53	-	342.60	349.44	-	370.43	
8	HORIZONTAL BEND	DUCTED			8.00	224.13	31.29	0.20	748.45	3.34	373.90	310.64	1.39	350.43	
9	STRAIGHT PULL	DUCTED	71.24					0.20	886.66	-	445.14	249.43		319.13	
10	HORIZONTAL BEND	DUCTED			17.00	126.12	37.42	0.20	977.93	7.75	482.56	783.75	6.21	247.89	
11	STRAIGHT PULL	DUCTED	68.31					0.20	1110.45	-	550.87	698.86	-	210.47	1
12	HORIZONTAL BEND	DUCTED			98.00	10.45	17.87	0.20	1565.00	149.76	568.74	566.34	54.19	142.16	_
13	UPWARD SLOPE	DUCTED	20.70	9.00				0.20	1636.07	-	589.44	399.12	-	124.29	-
14	HORIZONTAL BEND	DUCTED			42.00	6.34	4.65	0.20	1894.57	298.83	594.09	328.05	51.74	103.59	+
15	UPWARD SLOPE	DUCTED	24.10	11.00				0.20	1985.07	-	618.19	282.47	-	98.94	+
16	HORIZONTAL BEND	DUCTED			26.00	6.43	2.92	0.20	2173.75	338.06	621.11	191.97	29.86	74.84	
17	UPWARD SLOPE	DUCTED	8.65	15.00				0.20	2211.68	-	629.76	174.42	-	71.92	
18	HORIZONTAL BEND	DUCTED			51.00	7.20	6.41	0.20	2642.83	367.06	636.17	136.49	18.96	63.27	+
19	STRAIGHT PULL	DUCTED	10.44		00.00	00.00	0.00	0.20	2663.08	-	646.61	111.22	-	56.87	+
20 21	HORIZONTAL BEND STRAIGHT PULL	DUCTED	37.35		20.00	26.00	9.08	0.20	2856.47 2928.93	109.86	655.68 693.03	90.97 72.46	3.50	46.43 37.35	+
		DUCTED	37.35			-		0.20		-	093.03		-		+
0	ENTRY/EXIT TENSION	1						1 - 1	2928.93	367.06		0	0	0	1

Figure 3 Cable Pulling Calculation - JB24-JB25

On review of the pinch point section highlighted within JB25-JB26. The cable pulling study analysis found that installing an **NKT 1600mm<sup>2</sup> AL XLPE (110kV) UGC** from JB26 and carrying predominantly in a downward gradient to the location of Joint Bay 25. The result of the approximate pulling exit tension value would be **3453.24kg**.

It was found during analysis when installing the cable from JB25, carrying in an upward gradient to the location of Joint Bay 26, the permissible pulling force exerted onto the cable exceeded the manufactures specified limit of 4894.56kg. The pulling tension value for this prospective install resulted in approx. **7304.48kg** 



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The cable pulling study findings for the maximum permissible sidewall force allowable were found to be within the specified limits with approx. **240.95kg/m** when installed from JB26 (downhill).

Findings show approx. **1340.97kg/m** of force exerted for the Side Wall Pressure analysis when the cable is installed from JB25 (uphill) respectively exceeding the specified limit of 1019.7kg/m

tli <sup>))))</sup> group															
SECTIC	DN DETAILS														
01001117	Ardnacrusha -														
CIRCUIT	Carrownagowan														
ROUTE SECTION	4														
CABLE SECTION	JB25-JB26														
FROM	JB25														
то	JB26														
	DN PARAMETERS														
CABLE WEIGHT (kg/m)															
C.O.F. (DUCT)	0.2														
PULL TYPE	NOSE PULL														
			STRAIGHT S	ECTION	в	END SECTIO	)N	COF			CALCULATIO				REMARKS
OF OUT UT UO		DUOTED DIDEOT DUDI U						LOF	JB25	TO	JB26	JB26	TO	JB25	REMARKS
SEGMENT NO.	SEGMENT TYPE	DUCTED/DIRECT BURIAL	LENGTH	SLOPE	BEND ANGLE				NOSE TENSION	S₩P	CHAINAGE	NOSE TENSION	SWP	CHAINAGE	
			m	deg	deg	m	m		kg	kgim	m	ky	kynim	m	
0	ENTRY/EXIT TENSION								0	0	0	7304.48	1340.97	-	
1	STRAIGHT PULL	DUCTED	7.79					0.20	15.11	-	7.79	7304.48	-	676.30	
2	HORIZONTAL BEND	DUCTED			26.00	5.86	2.66	0.20	20.52	3.50	10.45	7289.37	1243.92	668.51	
3	STRAIGHT PULL	DUCTED	2.94	0.00			0.00	0.20	26.22	-	13.39	6656.92	-	665.85	
4	HORIZONTAL BEND	DUCTED			31.00	4.96	2.68	0.20	32.32	6.52	16.07	6651.21	1340.97	662.91	
5	STRAIGHT PULL	DUCTED	14.52	1.00			0.00	0.20	62.94	-	30.59	5969.04	-	660.23	
6	HORIZONTAL BEND	DUCTED			42.00	4.96	3.64	0.20	75.28	15.18	34.23	5938.42	1197.26	645.71	
7	STRAIGHT PULL	DUCTED	13.74	2.00			0.00	0.20	106.57	-	47.97	5128.58	-	642.07	
8	HORIZONTAL BEND	DUCTED			16.00	18.26	5.10	0.20	118.28	6.48	53.07	5097.29	279.15	628.33	
9	STRAIGHT PULL	DUCTED	9.80	0.00			0.00	0.20	137.29	-	62.87	4820.24	-	623.23	
10	HORIZONTAL BEND	DUCTED			15.00	24.20	6.34	0.20	151.73	6.27	69.20	4801.22	198.40	613.43	
11	UPWARD SLOPE	DUCTED	23.15	9.00			0.00	0.20	231.21	-	92.35	4556.00	-	607.10	
12	HORIZONTAL BEND	DUCTED			14.00	13.02	3.18	0.20	244.37	18.77	95.53	4476.51	343.82	583.95	
13	UPWARD SLOPE	DUCTED	6.12	10.00			0.00	0.20	266.37	-	101.65	4262.92	-	580.77	
14	HORIZONTAL BEND	DUCTED			96.00	13.75	23.04	0.20	383.17	27.87	124.69	4240.92	308.43	574.65	
15	STRAIGHT PULL	DUCTED	26.40	3.00			0.00	0.20	447.72	-	151.09	3032.66	-	551.61	
16	HORIZONTAL BEND	DUCTED			89.00	9.33	14.49	0.20	613.70	65.78	165.59	2968.12	318.13	525.21	
17	UPWARD SLOPE	DUCTED	111.30	7.00			0.00	0.20	959.59	-	276.89	2175.07	-	510.71	
18	HORIZONTAL BEND	DUCTED	44.40		42.00	6.60	4.84	0.20	1111.42	168.40	281.72	1829.18	277.15	399.41	
19 20	UPWARD SLOPE	DUCTED	11.16	6.00	23.00	13.36	0.00	0.20	1144.26 1240.51	- 92.85	292.88 298.25	1579.58 1546.73	- 115.77	394.58	
20	HORIZONTAL BEND UPWARD SLOPE	DUCTED	11.72	6.00	23.00	10.36	5.36	0.20	1240.51	92.85	298.25	1426.97		383.42 378.05	
21	HORIZONTAL BEND	DUCTED	11.72	6.00	16.00	9.04	2.52	0.20	1275.00	- 149.16	309.97	1426.97	- 154.03	378.05	1
22	UPWARD SLOPE	DUCTED	27.44	8.00	10.00	3.04	2.52	0.20	1348.41	143.16	312.49	1392.47	154.03	365.33	
23	HORIZONTAL BEND	DUCTED	21.99	0.00	23.00	13.04	5.23	0.20	1436.17	- 119.54	335.53	1226.92	94.09	336.37	1
24	UPWARD SLOPE	DUCTED	7.67	7.00	23.00	10.04	5.23	0.20	1582.67	- 113.54	345.17	1226.32	34.03	330.37	1
25	HORIZONTAL BEND	DUCTED	1.07	1.00	39.00	10.02	6.82	0.20	1813.89	- 181.03	359.66	1107.91	96.44	323.46	
20	UPWARD SLOPE	DUCTED	21.84	7.00	35.00	10.02	0.02	0.20	1881.77	-	381.50	966.32		316.64	1
28	HORIZONTAL BEND	DUCTED	21.04	1.00	39.00	8.95	6.09	0.20	2156.47	240.95	387.59	898.45	87.54	294.80	
29	STRAIGHT PULL	DUCTED	41.91	5.00	35.00	0.00	0.00	0.20	2130.47	240.33	429.50	783.52	- 01.34	288.71	1
30	HORIZONTAL BEND	DUCTED		0.00	11.00	21.11	4.05	0.20	2362.22	111.90	433.55	667.10	30.35	246.80	
31	UPWARD SLOPE	DUCTED	56.98	6.00			0.00	0.20	2529.93	-	490.53	640.79	-	242.75	
32	HORIZONTAL BEND	DUCTED	00.00	0.00	20.00	22.48	7.85	0.20	2713.52	120.71	498.38	473.08	19.48	185.77	1
33	STRAIGHT PULL	DUCTED	87.03	4.00	20.00		0.00	0.20	2940.84	-	585.41	437.84	-	177.92	
34	HORIZONTAL BEND	DUCTED			33.00	52.49	30.23	0.20	3304.93	62.96	615.64	210.52	2.83	90.89	
35	STRAIGHT PULL	DUCTED	60.66	3.00			0.00	0.20	3453.24	-	676.30	148.31	-	60.66	
0	ENTRY/EXIT TENSION				-				3453.24	240.95	-	0	0	0	

Figure 4 Cable Pulling Calculation - JB25-JB26

On review of the pinch point section highlighted within JB27-JB28. The cable pulling study analysis found that installing an **NKT 1600mm<sup>2</sup> AL XLPE (110kV) UGC** from either side would result in approximate pulling tension values of **2609.7kg** and **3295.44kg** respectively in keeping with the manufactures specified limit of 4894.56kg.

The cable pulling study also found consistent values for the maximum permissible sidewall force allowable with approx. **107.71kg/m** when installed from JB27 and approx. **274.79kg/m** when installed from JB28. This ensures that the maximum pulling tension and side wall bearing pressure limits of the cable to be installed would not be exceeded during construction based on the current design.



Project: Carrownagow	an WF – 110kV Grid Connection	Ref: Rev2	
Section: UG Cable Pul	ling Calculation Check	Job No: 05-641	
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SECTION	DETAILS														
CIRCUIT	Ardnacrusha - Carrownagowan														
ROUTE SECTION	4														
CABLE SECTION	JB27-JB28														
FROM	JB27														
TO	JB28														
10	0020														
CALCULATION	PARAMETERS														
CABLE WEIGHT (kg/m)	9.7														
C.O.F. (DUCT)	0.2														
PULL TYPE	NOSE PULL														
			CTDA	ICUT		DEND					CALCULATI	ON RESULTS			
			STRA	IGHT		BEND		COF	JB27	TO	JB28	JB28	TO	JB27	REMARKS
SEGMENT NO.	SEGMENT TYPE	DUCTED/DIRECT BURIAL	LENGTH	SLOPE	BEND ANGLE	RADIUS	ARC LENGTH	1	NOSE TENSION	SWP	CHAINAGE	NO SE TEN SION	SWP	CHAINAGE	
			m	deg	dea	m	m		ka	ka/m	m	ka	ka/m	m	
0	ENTRY/EXIT TENSION	-	-	-	-	-	-	-	0	0	Ö	3295.44	274.79	-	
1	STRAIGHT PULL	DUCTED	10.09					0.20	19.57		10.09	3295.44		653.34	
2	HORIZONTAL BEND	DUCTED	10.05		29.00	15.60	7.90	0.20	35.15	2.25	17.99	3275.86	209.99	643.25	
3	STRAIGHT PULL	DUCTED	49.06	5.00	20.00	10.00	1.00	0.20	171.44		67.05	2960.13	-	635.36	
4	HORIZONTAL BEND	DUCTED	10.00	0.00	41.00	21.16	15.14	0.20	211.60	10.00	82.19	2823.84	133.45	586.30	
5	STRAIGHT PULL	DUCTED	4.55	0.00	41.00	21.10	10.11	0.20	220.43	-	86.74	2446.22	-	571.16	
6	HORIZONTAL BEND	DUCTED	4.00	0.00	42.00	8.87	6.50	0.20	257.62	29.04	93.24	2437.39	274.79	566.61	
7	UPWARD SLOPE	DUCTED	14.20	9.00	42.00	0.01	0.00	0.20	306.37	20.04	107.44	2104.79	-	560.11	
8	HORIZONTAL BEND	DUCTED	11.20	0.00	24.00	20.72	8.68	0.20	338,18	16.32	116.12	2056.03	99.23	545.91	
9	UPWARD SLOPE	DUCTED	10.70	12.00	21.00	20.12	0.00	0.20	380.06	-	126.82	1889.98	-	537.23	
10	HORIZONTAL BEND	DUCTED	10.10	12.00	72.00	11.57	14.54	0.20	492.78	42.59	141.36	1848.10	159.73	526.53	
11	STRAIGHT PULL	DUCTED	41.15	5.00				0.20	607.10	-	182.51	1436.53	-	511.99	
12	HORIZONTAL BEND	DUCTED			18.00	60.64	19.05	0.20	661.44	10.91	201.56	1322.21	21.80	470.84	
13	STRAIGHT PULL	DUCTED	59.95	5.00				0.20	827.99	-	261.51	1233.83	-	451.79	
14	HORIZONTAL BEND	DUCTED	-		18.00	45.21	14.20	0.20	888.53	19.65	275.71	1067.29	23.61	391.84	
15	UPWARD SLOPE	DUCTED	182.54	7.00				0.20	1455.80	-	458.25	996.85	-	377.63	
16	HORIZONTAL BEND	DUCTED			23.00	14.90	5.98	0.20	1578.08	105.91	464.23	429.58	28.83	195.09	
17	STRAIGHT PULL	DUCTED	6.69	0.00				0.20	1591.06	-	470.92	394.53	-	189.11	-
18	HORIZONTAL BEND	DUCTED			21.00	15.90	5.83	0.20	1712.62	107.71	476.75	381.56	24.00	182.42	
19	STRAIGHT PULL	DUCTED	16.42	0.00				0.20	1744.47	-	493.17	352.39	-	176.59	
20	HORIZONTAL BEND	DUCTED			12.00	66.01	13.83	0.20	1823.86	27.63	507.00	320.53	4.86	160.17	
21	STRAIGHT PULL	DUCTED	17.94	0.00				0.20	1858.67	-	524.94	290.81	-	146.35	
22	HORIZONTAL BEND	DUCTED			18.00	55.75	17.51	0.20	1984.04	35.59	542.45	256.01	4.59	128.41	
23	STRAIGHT PULL	DUCTED	15.78	0.00				0.20	2014.66	-	558.23	218.89	-	110.89	
24	HORIZONTAL BEND	DUCTED			47.00	50.75	41.63	0.20	2383.61	46.97	599.86	188.28	3.71	95.11	
25	STRAIGHT PULL	DUCTED	23.49	0.00				0.20	2429.18	-	623.35	103.96	-	53.48	
26	HORIZONTAL BEND	DUCTED			16.00	34.07	9.51	0.20	2569.96	75.43	632.86	58.39	1.71	29.99	
27	STRAIGHT PULL	DUCTED	20.48	0.00				0.20	2609.69		653.34	39.73	1.1	20.48	
0	ENTRY/EXIT TENSION	-	-	-	-	-	-	-	2609.7	107.71	-	0	0	0	

Figure 5 Cable Pulling Calculation - JB27-JB28

### **Appendix A – Functional Cable Specification**

# EIRGRID

110kV Underground Cable Technical Schedules

NK7

#### SCHEDULE A (continued)

#### Physical Characteristics of 110 kV Crosslinked Polyethylene Cable

Item	Query	Required	Offered
10	Nominal diameter of completed cable (mm)		96
11	Weight of finished cable (kg/m)		appr. 9,7
12	(a) Normal length per drum (m)		1000
	(b) Maximum length per drum (m)		tbd
13	<ul><li>(a) Normal gross weight of loaded drum (kg)</li><li>(b) Max gross weight of loaded drum (kg)</li></ul>		12000 tbd
14	Drum dimensions width/height (m/m)		3,6 / 4,3
15	Minimum radius of bend around which cable can be pulled		
	(a) Laid direct (m)		2,4
	(b) In ducts (m)		2,4
	(c) Cable placed in position with former (m)		1,5
	(d) Cable placed in position without former (m)		2,4
16	Permissible pulling force allowed on conductors during installation (kN)		48
			-10
17	Maximum permissible sidewall forces (kN/m)		10

### Carrownagowan WF - 110kV Grid Connection

### Route Summary & Joint Bay Locations

Rev3 (27.03.20)

Section From	Section To	Section Length	Bonding Arrangement	No. of Watercourses	Watercourses	No. of Bridges	Bridges	Comments	D
SS	JB-1	542	Single Point Bonded	-	-	-	-	Route into SS to be determined by ESB	
JB-1	JB-2	570	Cross Bonded	-	-	-	-		1
JB-2	JB-3	561	Cross Bonded	-	-	-	-		
JB-3	JB-4	554	Cross Bonded	1	C1	-	-		
JB-4	JB-5	673	Cross Bonded	-	-	-	-		3
JB-5	JB-6	638	Cross Bonded	-					
JB-6	JB-7	673	Cross Bonded	-					
JB-7	JB-8	688	Single Point Bonded	1	B1	1	B1	B1 to be HDD	
JB-8	JB-9	620	Cross Bonded	1	B2	1	B2		
JB-9	JB-10	660	Cross Bonded	1	C2	-			
JB-10	JB-11	641	Cross Bonded	2	C3,B3	1	B3		
JB-11	JB-12	807	Cross Bonded	-					
JB-12	JB-13	782	Cross Bonded	2	C4,C5				
JB-13	JB-14	789	Cross Bonded	-					
JB-14	JB-15	742	Cross Bonded	-					
JB-15	JB-16	722	Cross Bonded	1	C6				
JB-16	JB-17	760	Cross Bonded						
JB-17	JB-18	768	Cross Bonded	1	С7				
JB-18	JB-19	762	Cross Bonded	-					
JB-19	JB-20	730	Cross Bonded	1	B4	1	B4		
JB-20	JB-21	822	Cross Bonded	2	C8,B5	1	B5		
JB-21	JB-22	789	Cross Bonded	1	B6	1	B6		
JB-22	JB-23	798	Cross Bonded	2	C9,B7	1	B7		
JB-23	JB-24	703	Cross Bonded	2	B8,B9	2	B8,B9		
JB-24	JB-25	698	Cross Bonded	-					
JB-25	JB-26	680	Cross Bonded	-					
JB-26	JB-27	670	Cross Bonded	-					
JB-27	JB-28	672	Cross Bonded	-					
JB-28	JB-29	681	Cross Bonded	-					
JB-29	JB-30	749	Cross Bonded	3	C10,C11,C12				
JB-30	JB-31	751	Cross Bonded	4	C15,C16,C17,C18				
JB-31	JB-32	752	Cross Bonded	1	C19				
JB-32	JB-33	749	Cross Bonded	3	C22,C23,C24				
JB-33	JB-34	752	Cross Bonded	1	C25	1			
JB-34	JB-35	749	Cross Bonded	4	C26,C27,C28,C29				
JB-35	WF SS	267	Single Point Bonded						
JB-35	WF SS	267	Single Point Bonded						
	Total	: 24,964		34		9			=



Outline Construction Methodology – 110kV Underground Cable Connection



Carrownagowan Wind Farm Grid Connection



Report Ref: 05641-R03-03

Client: Coillte C/o Malachy Walsh Partners







Revision:	Author:	Checked:	Date:	Notes:
00	DB	SK	04.03.19	Issued for Client Review
01	SK	RG	29.11.19	Revised Substation Location
02	SK	RG	27.03.20	Revised following Client Review
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#### **1.0 Introduction**

The purpose of this document is to outline and explain the construction techniques and methodologies which will be implemented during construction of the proposed Carrownagowan Wind Farm 110kV grid connection to the existing ESB Ardnacrusha 110kV substation. The grid connection will consist entirely of underground cabling (UGC) with the majority of the UGC to be installed within the public road network.

The UGC works will consist of the installation of 5 No. ducts in an excavated trench to accommodate 3 No. power cables, and 1 No. fibre communications cable to allow communications between the Carrownagowan Wind Farm Substation and Ardnacrusha 110kV substation.

This document is intended to be used as an aid to understand the methodologies to be employed during construction and should be read in conjunction with all other specialist reports which accompany the planning application. In addition, this document is in outline form only and will be revised and updated prior to the commencement of any construction activities, detailed Method Statements will be prepared in respect of each aspect of the proposed development.

#### 2.0 Proposed 110kV Underground Cable Route

The proposed UGC route is approximately 25km in length and runs in a northerly direction from the existing ESB Ardnacrusha 110kV substation to the proposed Carrownagowan Wind Farm substation location utilizing public local road networks, existing access tracks and private forestry access tracks.

The exact location of the UGC within the proposed site boundary is subject to minor modification following a further detailed assessment to be undertaken prior to construction and following consultation with Clare County Council and all other relevant stakeholders, having regard to all environmental protection measures outlined in the planning application and accompanying technical reports.

Below (Figure 1) which outlines the proposed UGC route, with each section of the route being formulated in detail within Table 1.

This proposed grid connection option is shown as an Overall Site layout Plan in Drawing No. 05641-200.





Figure 1 - Grid Connection Route Location

**Table 1** of this report summaries the route location features of the underground cable connection and proposedroute.

Table 1 – Approximate Route Location of Preliminary Design:		
Wind Farm Site/Forestry Roads (UGC)	Public Roads (UGC)	ESB Access Track (UGC)
5,504 m	18,875 m	585 m

Table 1: Carrownagowan Wind Farm to Ardnacrusha 110kV Substation – UGC Route Location Summary

Table 2 below separates the UGC route into a number of sections and describes the specific construction requirements of each individual section with access routes to the work areas. All plant and equipment employed



on the proposed works will be subject to good site organisation and hygiene, particularly during construction activities.

Table 2 - Summary of Preliminary Grid Connection Design Route		
Section	Description	
Section 1	UGC from Ardnacrusha 110kV substation to R-471 Road	
UGC 3,538 m	The proposed underground cable route initially begins within the Ardnacrusha substation compound exiting the confines northerly provisionally turning right onto the local public route of the (L-3056).	
	Approaching a crossroad junction, the UGC turns left opposite the main entrance of Ardnacrusha Power Station onto Lackyle Heights Rd and continuing along this route for approx. 2.8km. The UGC will predominantly be installed in the carriageway until encountering another road junction at which point the UGC will turn right onto an unpaved section of roadway.	
	The UGC will continue north on this unpaved road where it will encounter the first proposed bridge crossing within the proposed route over the River Blackwater (Bridge 1). This bridge will be crossed using a horizontal directional drill method (HDD) before continuing along this unpaved section of roadway for approx. 1.37km.	
	<u>Features</u>	
	Section 1 contains 7 no. joint bays. Joint bays will be located below ground and finished/reinstated to the required roads specification. Joint bays will have associated communication chambers and link boxes which will have a surface access hatch which will match existing ground levels.	
	<ul> <li>Joint Bay 01 (JB01) will be located approx. 542m north of Ardnacrusha 110kV Substation. The joint bay will be installed within the local public network west of the Power Station entrance road.</li> </ul>	
	<ul> <li>Joint Bay 02 (JB02) will be located approx. 570m north of JB01 within the local road network situated within Lackyle Road</li> </ul>	
	<ul> <li>Joint Bay 03 (JB03) will be located approx. 561m north of JB02 positioning the joint bay within the Lackyle Rd network.</li> </ul>	
	<ul> <li>Joint Bay 04 (JB04) will be located approx. 554m north of JB03. The position of JB04 will be located approx. 415m after departing Lackyle road positioned to an entrance to agricultural grassland.</li> </ul>	
	<ul> <li>Joint Bay 05 (JB05) will be located approx. 673m north of JB04 within the local authority carriageway. The joint bay will be situated adjacent to an uninhabited dwelling with the positioning within the shoulder of the roadway.</li> <li>Joint Bay 06 (JB06) is located 638m northwest of JB05 within the shoulder of an unpaved section of roadway.</li> </ul>	



	<ul> <li>Joint Bay 07 (JB07) will be located approx. 673m north of JB06 adjacent to a gated agricultural entrance within this unpaved carriageway. JB07 is located immediately south of the first proposed Bridge crossing.</li> <li>Section 1 has 1 bridge crossing:</li> <li>The proposed route crosses over the River Blackwater. Insufficient clearance exists within the bridge structure and it is proposed to cross this bridge adopting the HDD method before proceeding towards the (R-471). The HDD crossing will require a transition coupler to be installed at either side of the drill following the works, the location of these couplers is to be determined by the drilling contractor following site investigation.</li> </ul>
Section 2	UGC within R-471 and L-3046 Carriageway
UGC 7,206 m	Subsequent to this unpaved section of roadway, the UGC comes upon the regional road (R-471) with the prospective installation merging and turning right onto the regional carriageway heading in an eastward direction.
	The underground cable will continue eastwards passing first the church of Truagh before encountering a junction that will require the UGC to cross both lanes of a merging roadway after circa 372m before continuing along the (R-471). Within the regional road, the first of two-bridge crossings in this section exists after 172m (Bridge 2). Continuing on for a further circa 664m prior to approaching the regional road (R-465). At this junction the UGC will be required to cross underground services (Water, Telecoms, etc) which are evident within the surrounding layout and the lanes of carriageway proceeding straight along the (R-471). Subsequent to cable trenching along this route for circa. 453m, the UGC reaches the second proposed bridge crossing of the Glenmora Wood Stream (Bridge 3) which will be crossed using HDD. Once the UGC crosses this structure, the route continues for a further circa 905m before turning left onto a local route (L-3046) leaving the (R-471) carriageway. The underground cable will carry along this route on the (L-3046) for approximately 4.24km.
	<u>Features</u>
	Section 2 contains 10 no. joint bays. Joint bays will be located below ground and finished/reinstated to the required national roads specification. Joint bays will have associated communication chambers and link boxes which will have a surface access hatch which will match existing ground levels.
	<ul> <li>Joint Bay 08 (JB08) will be located 689m after JB07 on the regional road (R-471) within the shoulder of this roadway prior to entering Truagh. An existing ESB MV OHL crosses this (R-471) roadway 107m east of JB07</li> <li>Joint Bay 09 (JB09) will be located within the (R-471) roadway, approx. 620m east of JB08. Noted is an OHL MV line running parallel to the (R-471)</li> </ul>



	<ul> <li>Joint Bay 10 (JB10) will be located within the (R-471) roadway, approx. 660m east of JB09 and 208m subsequent to crossing the regional carriageway (R-465).</li> <li>Joint Bay 11 (JB11) will be located within the (R-471) roadway approx. 640m southeast of JB10. The Joint bay will reside within a gated agricultural entrance.</li> <li>Joint Bay 12 (JB12) will be located within the (L-3046) local roadway, approx. 807m east of JB11. JB11 is located north of the (R-471) post a road junction.</li> <li>Joint Bay 13 (JB13) will be located within the (L-3046) local roadway, approx. 782m north of JB12.</li> <li>Joint Bay 14 (JB14) will be located within the (L-3046) local roadway, approx. 789m north of JB13.</li> <li>Joint Bay 15 (JB15) will be located within the (L-3046) roadway approx. 782m north east of JB14. The Joint bay will reside adjacent to a gated forestry access entrance.</li> <li>Joint Bay 16 (JB16) will be located within the (L-3046) local roadway, approx. 764m north of JB15.</li> </ul>
	Section 2 has 2 bride crossing:
	• The first bridge crosses over the Glenmora Wood Stream within the (R-471) approx. 160m prior to encountering JB09. Insufficient clearance exists within the bridge structure and it is proposed to cross this bridge utilizing the HDD method.
	• The second bridge crossing again exists within the (R-471) carriageway and is situated approx. 238m subsequent to JB10. The structure is twin arched and crossing by means of HDD will be utilized.
Section 3	UGC within R-466 Carriageway, local roadway, Kilbane Village
OHL 6,140 m	Section 3 of the grid connection route joins onto the regional route (R-466) which requires passing two lanes of roadway at this junction before continuing for another circa 644m of carriageway before leaving this regional route onto a local public route. The UGC route carries for circa 474m, before encountering a fourth bridge (Bridge 4). This crossing will be carried out by means of installing the UGC within the bridge deck as it has been found that sufficient cover exists in the structure. Continuing along the proposed route for approx. 1.06km, a fifth proposed bridge (Bridge 5) crossing over the Glenomra River which will be crossed using HDD. On passing this structure the UGC continues for another circa. 903m to encounter a sixth bridge crossing over the along the proposed route which is situated within the small village area of Kilbane (Bridge 6), this bridge will also be crossed using HDD. Once passed the bridge structure over the crossed over the Kilbane stream, the UGC exits the Kilbane village and heads in a north-westerly direction past the townland of Upper Kilbane until the proposed route encounter a seventh bridge crossing over the Clonagaheen east stream (Bridge



443m after the subsequent which crosses over the Clonagaheen west stream (Bridge 8), it is proposed to cross this bridge using HDD. The final bridge structure is situated circa 215m after the previous which crosses over O'Shea's Acres stream (Bridge 9).

#### <u>Features</u>

Section 3 contains 7 No. joint bays. Joint bays will be located below ground and finished/reinstated to the required national roads specification. Joint bays will have associated communication chambers and link boxes which will have a surface access hatch which will match existing ground levels.

- Joint Bay 17 (JB17) will be located approx. 768m north east of JB16 on the regional road of the (R-466)
- Joint Bay 18 (JB18) will be located within a paved local roadway, approx. 768m north east of JB17 and approx. 360m subsequent to the regional road (R-466). The Joint Bay will reside within a gated entrance to agricultural parcel.
- Joint Bay 19 (JB19) will be located within this paved local roadway, approx. 762m north of JB18. Prior to encountering this Joint Bay location, the UGC route will be required to cross beneath an existing TSO 400kV OHL transmission line, approx. 115m before JB19.
- Joint Bay 20 (JB20) will also be located within this paved local roadway, approx.
   730m north of JB19.
- Joint Bay 21 (JB21) will also be located within this paved local roadway, approx. 822m north west of JB20. JB21 is located approx. 260m north of Kilbane village.
- Joint Bay 22 (JB22) will also be located within this paved local roadway, approx.
   789m west of JB21. The Joint bay will reside within a shouldered road junction within this paved carriageway.
- Joint Bay 23 (JB23) will also be located within this paved local roadway, approx. 798m west of JB22.

Section 3 has 6 bridge crossings:

- The first bridge crossing within this section is (Bridge 4). This crossing will be carried out by means of installing the UGC within the bridge deck as it has been found that sufficient cover exists in the structure.
- The second bridge in this section is (Bridge 5) where the bridge crosses over the Glenmora River. Insufficient clearance exists within the bridge structure and it is proposed to cross this bridge adopting the HDD method before proceeding.
- The third bridge crossing within this section is (Bridge 6), where the proposed route crosses over a watercourse within the village of Kilbane. Insufficient clearance exists within the bridge structure and it is proposed to cross this bridge adopting the HDD method before proceeding.
- The forth bridge crossing within the section is (Bridge 7), where the UGC route crosses over the Clonagaheen east stream. Sufficient clearance exists within



	the bridge structure and it is proposed to cross this bridge within the deck of a new raised road level.
	• The fifth bridge crossing within this section is (Bridge 8), where the roadway crosses over the Clonagaheen west stream. Insufficient clearance exists within the bridge structure and it is proposed to cross this bridge adopting the HDD method before proceeding.
	• The sixth bridge crossing within this section is (Bridge 9), this structure is the crossing point over O'Shea's Acres stream. Insufficient clearance exists within the bridge structure and it is proposed to cross this bridge adopting the HDD method before proceeding towards the Windfarm site.
Section 4	UGC within Access Roadway to Windfarm
UGC 8,080 m	The UGC route continues along the local road subsequent to Joint bay 23 for an additional 600m in a westerly direction until reaching a local roadway on the right-hand side.
	Thus, the UGC accesses this route and continues uphill for approximately 1.74km before the road becomes unpaved. From this point on, the unpaved roadway forms a forestry access track continuing in a northerly direction. On this route, the cable accesses the proposed Carrownagowan Wind Farm site boundary within, carrying on the use of these forestry access tracks further for approximately 5km until reaching the proposed location for the Independent Power Provider (IPP) substation.
	<u>Features</u>
	Section 4 contains 13 no. joint bays. Joint bays will be located below ground and finished/reinstated to the required roads specification or landowner requirements. Joint bays will have associated communication chambers and link boxes which will have a surface access hatch which will match existing ground levels.
	• Joint Bay 24 (JB24) will be located approx. 703m after JB23 on this access roadway heading in a north westerly direction.
	<ul> <li>Joint Bay 25 (JB25) will be located within the access roadway, approx. 701m north of JB24.</li> <li>Joint Bay 26 (JB26) will be located within this access roadway also the joint bay will be set up approx. 681m after JB25 in a north westerly direction heading towards the Windfarm.</li> </ul>
	<ul> <li>Joint Bay 27 (JB27) will be located approx. 670m after JB26, at this point the roadway will have become unpaved prior to accessing the privately-owned forestry lands.</li> </ul>
	• Joint Bay 28 (JB28) will be located within this unpaved section and will have accessed the privately-owned forestry. Its location will exist approx. 674m north of JB27.
	• Joint Bay 29 (JB29) will be located within the privately-owned forestry access trackway approx. 681m north after JB28.



	<ul> <li>Joint Bay 30 (JB30) will be located within the windfarm access track approx 749m north east of JB29.</li> <li>Joint Bay 31 (JB31) will exist within the proposed windfarm access track approx 751m north east of JB30.</li> <li>Joint Bay 32 (JB32) will exist within the proposed windfarm access track approx 752m north east of JB31.</li> <li>Joint Bay 33 (JB33) will exist within the proposed windfarm access track approx 749m north east of JB32.</li> <li>Joint Bay 34 (JB34) will exist within the proposed windfarm access track approx 752m north east of JB32.</li> <li>Joint Bay 35 (JB35) will exist within the proposed windfarm access track approx 752m north east of JB33.</li> <li>Joint Bay 35 (JB35) will exist within the proposed windfarm access track approx 749m north east of JB34. JB35 is approx. 267m outside of the windfarm substation.</li> </ul>
Refer to Figure 1	and to the planning drawings submitted for location details.
_	e location of the proposed route within the planning application boundary is subject to change
-	ng services/utility locations, ground conditions and any environmental constraints.

#### 3.0 Access Routes to Work Area

The majority of the proposed underground cable will be installed within the public road network and therefore will be accessed via the existing road network. Where the cable route is located on private lands, contractor(s) will be required to utilise the local public road network in the vicinity of the work area and from there utilise private access tracks, where appropriate.

A detailed Traffic Management Plan will be prepared, and agreed with Clare County Council, prior to the commencement of construction. Some work areas will require a road closure where it is not possible to safely implement a Stop/Go system. Where road closures are necessary, a suitable diversion will be implemented using appropriate signage, following consultation with Clare County Council.

Careful and considered local consultation will be carried out, to minimise the amount of disturbance caused during works. Prior to the commencement of construction, the contractor will assess all access routes and determine any additional access requirements which will be incorporated as part of the method statement. All plant and equipment employed during the proposed works (e.g. diggers, tracked machines, footwear etc.) will be inspected prior to arrival on site and on leaving site and cleaned where necessary to prevent the spread of invasive aquatic / riparian species.

#### 4.0 Traffic Management

Traffic management and road signage will be in accordance with the Department of Transport: Traffic Signs Manual - Chapter 8: Temporary Traffic Measures and Signs for Road Works and in agreement with Clare County

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Council. All work on public roads will be subject to the approval of a road opening license application. The contractor will prepare detailed traffic management plans for inclusion as part of the road opening applications. Where road widths allow, the UGC installation works will allow for one side of the road to be open to traffic at all times by means of a 'Stop/Go' type traffic management system, where a minimum 2.5m roadway will be maintained at all times. Where it is not possible to implement a 'Stop/Go' system a full road closure will be required. Temporary traffic signals will be implemented to allow road users safely pass through the works area by channelling them onto the open side of the road. Typically, the UGC will be installed in 100m sections, and no more than 100m will be excavated without the majority of the previous section being reinstated. Where the construction requires the crossing of a road, works on one carriageway will be completed before the second carriageway is opened, to maintain traffic flows.

All construction vehicles will be parked within the works area so as not to cause additional obstruction or inconvenience to road users or residents. The traffic signals will be in place prior to the works commencing and will remain in place until after the works are completed. The public road will be checked regularly and maintained free of mud and debris. Road sweeping will be carried out as appropriate to ensure construction traffic does not adversely affect the local road condition.

In the event of emergency; steel plates, which will be available on site, can be put in place across the excavation to allow traffic to flow on both sides of the road.

All traffic management measures will comply with those outlined in the accompanying Traffic Management Report and will be incorporated into a detailed Traffic Management Plan to be prepared, in consultation with Clare County Council, prior to the commencement of development.

# 5.0 Road Opening Licence

The proposed grid connection works will require a road opening licence under Section 254 of the Planning and Development Act 2000-2015 from Clare County Council. A Traffic Management Plan (TMP) will be agreed with Clare County Council prior to the commencement of the development. The TMP will outline the location of traffic management signage, together with the location of any necessary road closures and the routing of appropriate diversions. Where diversions are required, these will be agreed with Clare County Council in advance of the preparation of the TMP.

# 6.0 Construction Hours

Standard working hours for construction will be 8.00am to 8.00pm Monday to Friday and 8.00am to 6.00pm on Saturday (if required), with no works on Sundays or Bank Holidays except in exceptional circumstances or in the event of an emergency. All site personnel will be required to wear project notification labelling on high visibility vests and head protection so that they can be easily identified by all workers on-site.

# 7.0 UGC Construction Methodology

The proposed UGC will consist of 3 No. 160mm diameter HDPE power cable ducts and 2 No. 125mm diameter HDPE communications duct to be installed in an excavated trench, typically 600mm wide by 1,315mm deep, with variations on this design to adapt to bridge crossings, service crossings and watercourse crossings, etc. The



power cable ducts will accommodate 3 No. power cables. The communications duct will accommodate a fibre cable to allow communications between the Carrownagowan Wind Farm substation and Ardnacrusha 110kV substation. The ducts will be installed, the trench reinstated in accordance with landowner/Clare County Council specification, and then the electrical cabling/fibre cable is pulled through the installed ducts in approximately 650/750m sections. Construction methodologies to be implemented and materials to be used will ensure that the UGC is installed in accordance with the requirements and specifications of ESB.

# 7.1 Trenching Methodology

The following section outlines the methodology to be followed during trenching works:-

- The Contractor, and their appointed Site Manager, will prepare a targeted Method Statement concisely outlining the construction methodology and incorporating all mitigation and control measures included within the planning application and accompanying reports and as required by planning conditions where relevant;
- All existing underground services shall be identified on site prior to the commencement of construction works;
- At watercourse crossings, the contractor will be required to adhere to the environmental control measures outlined within the planning application and accompanying reports, the detailed Construction Environmental Management Plan (CEMP) to be prepared prior to the commencement of construction, and best practice construction methodologies;
- Where the cable route intersects with culverts, the culvert will remain in place (where possible) and the ducting will be installed either above or below the culvert to provide minimum separation distances in accordance with ESB and Irish Water specifications;
- In the event that culverts require removal for ducting installation, it is proposed that a suitable method of damming the water source and pumping the water around the work area would be set out in a method statement and agreed with the relevant stakeholders. Once the ducts are installed the culvert will be reinstated to match existing levels and dimensions. If works of this nature are required, the contractor will liaise with Inland Fisheries Ireland in advance of works;
- Traffic management measures will be implemented in accordance with those included in the Traffic Management Report, and a detailed Traffic Management Plan will be prepared and agreed with Clare County Council;
- Excavated material will be temporarily stockpiled onsite for re-use during reinstatement. Stockpiles will be restricted to less than 2m in height. Stockpiles will be located a minimum of 50m from surface water features and all stockpiling locations will be subject to approval by the Site Manager and Project Ecological Clerk of Works (ECoW);
- Excavated material shall be employed to backfill the trench where appropriate and any surplus material will be transported off site and disposed of at a fully authorised soil recovery site;
- Any earthen (sod) banks to be excavated will be carefully opened with the surface sods being stored separately and maintained for use during reinstatement;
- The excavated trench will be dewatered if required, from a sump installed within the low section of the opened trench. Where dewatering is required, dirty water will be fully and appropriately attenuated, through silt bags, before being appropriately discharged to vegetation or surface water drainage feature;

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- Where required, grass will be reinstated by either seeding or by replacing with grass turves;
- No more than a 100m section of trench will be opened at any one time. The second 100m will only be excavated once the majority of reinstatement has been completed on the first;
- The excavation, installation and reinstatement process will take on average of 1 no. day to complete a 100m section;
- Where the cable is being installed in a roadway, temporary reinstatement may be provided to allow larger sections of road to be permanently reinstated together;
- Following the installation of ducting, pulling the cable will take approximately 1 no. day between each joint bay, with the jointing of cables taking approximately 1 week per joint bay location.



Figure 2 Typical 110kV Underground Duct Installation

# 7.2 Ducting Installation Methodology

For the trenching and ducting works the following step by step methodology will apply:

- 1. Grade, smooth and trim trench floor when the required 1315mm depth and 600mm width have been obtained.
- 2. Place bedding layer of Cement Bound Granular Mixture B (CBGM B) material in accordance with the specification and compact it so that the compacted thickness is as per the drawings.
- 3. Lay the bottom row of ducts in trefoil formation as detailed on the design drawings. Use spacers as appropriate to establish horizontal duct spacing. Fit a secure cap / bung to the end of each duct run to prevent the ingress of dirt or water.
- 4. Carefully surround and cover ducts with CBGM B in accordance with the design drawings and specifications and thoroughly compact without damaging ducts.
- 5. Place cable protection strips on compacted CBGM B directly over the ducts.
- 6. Lay the top row of ducts onto the freshly compacted CBGM B including the cable protection strips above the bottom row of ducts. Place a secure cap at the end of each duct to prevent the ingress of dirt or water.



- 7. Carefully surround and cover ducts with CBGM B material in accordance with the drawings and thoroughly compact without damaging ducts.
- 8. Place red cable protection strip on top of compacted CBGM B over each set of ducts as shown on the drawings.
- 9. Place and thoroughly compact CBGM B material or Clause 804 backfill or soil backfill as specified and place warning tape at the depth shown on the drawings.
- 10.For concrete and asphalt/bitmac road sections, carry out immediate permanent reinstatement in accordance with the specification and to the approval of the local authority and/or private landowners, unless otherwise agreed with local authorities (Figure 3).
- 11.For unsurfaced/grass sections, backfill with suitable excavated material to ground level leaving at least 100 mm topsoil or match existing level at the top to allow for seeding or replace turves as per the specification of the local authority or landowner (Figure 4).
- 12.Clean and test the ducts in accordance with the specification by pulling through a brush and mandrel. Install 12 mm polypropylene draw rope in each duct and seal all ducts using robust duct end seals fitted with rope attachment eyes in preparation for cable installation at a later date. All the works should be witnessed by ESBN Clerk of Works (CoW) as required.

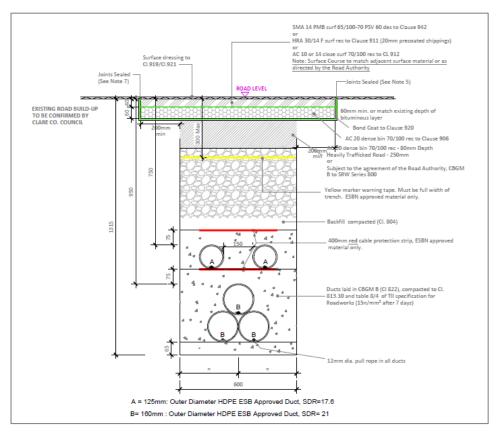


Figure 3 Typical Trench in Roadway



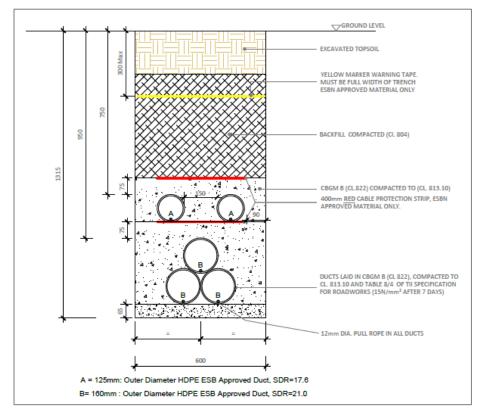


Figure 4 Typical Trench in Off Road Section

# Equipment:

- 2-3 General Operatives;
- 1 Excavator Operator;
- 1 no. tracked excavator (only rubber tracked machines will be allowed on public roads);
- 1 no. dumper or tractor and trailer.

# Materials:

- Sand for pipe bedding;
- Ready-mix Concrete where necessary (delivered to site);
- Trench backfilling material (excavated material and aggregates) to relevant specifications;
- 160mm diameter HDPE ducting;
- 125mm diameter HDPE ducting;
- Temporary Surface Reinstatement Materials

#### 7.2.1 On Public Road

The majority of the 110kV route is located within road carriages and where applicable the trench will be in the non-trafficked strip between the wheel marks on the road, presence of exiting utilities and the nature of the road and the adjoining terrain. It is preferable to excavate a trench within the middle of the lane, or the middle of the roadway to reduce load on the cable.

# Outline Construction Methodology 110kV Grid Connection – Carrownagowan Wind Farm May 2020



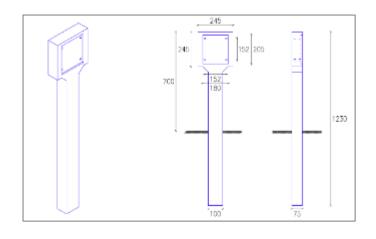
# 7.2.2 On Private Tracks

Where the cable is installed in private tracks the location where the cable is laid will depend on several factors, width of track, bends along the track and crossings. Where the track needs to be widened stone will be brought in to build up the area to the same level of the track. The excess material from the track will be used elsewhere on reinstatement works.

## 7.3 Marker posts

Surface cable markers will be placed along the route where cable depth is unavoidably shallow, due to constraints such as existing services, to indicate the precise location of the UGC. These markers will be metallic plates in accordance with ESB standards.

Marker posts will be used on non-roadway routes to delineate the cable route and joint bay positions. Corrosion proof aluminium triangular danger sign, with 700mm base, and with centred lightning symbol, on engineering grade fluorescent yellow background shall be installed in adequately sized concrete foundations. Marker post shall also be placed in the event that burial depth is not to standard. Siting of marker posts to be dictated by ESBN as part of the detailed design process. (Figure 5) below



#### Figure 5 Typical ESB Marker Posts Example

# 7.4 Horizontal Direction Drilling (HDD)

Horizontal Direction Drilling (HDD) is a method of drilling under obstacles such as bridges, railways, water courses, etc. in order to install cable ducts under the obstacle. This method is employed where installing the ducts using standard installation methods is not possible. There are a number of bridges on this UGC route which will require HDD due to there being insufficient cover and depth in the bridge to cross within the bridge deck. The proposed drilling methodology is as follows: -

- 1. A works area of circa .40m<sup>2</sup> will be fenced on both sides of the river crossing,
- 2. The drilling rig and fluid handling units will be located on one side of the bridge and will be stored on double bunded 0.5mm PVC bunds which will contain any fluid spills and storm water run-off.
- 3. Entry and exit pits (1m x 1m x 2m) will be excavated using an excavator, the excavated material will be temporarily stored within the works area and used for reinstatement or disposed of to a licensed facility.
- 4. A 1m x 1m x 2m steel box will be placed in each pit. This box will contain any drilling fluid returns from the borehole.



- 5. The drill bit will be set up by a surveyor, and the driller will push the drill string into the ground and will steer the bore path under the watercourse.
- 6. A surveyor will monitor drilling works to ensure that the modelled stresses and collapse pressures are not exceeded.
- 7. The drilled cuttings will be flushed back by drilling fluid to the steel box in the entry pit.
- 8. Once the first pilot hole has been completed a hole-opener or back reamer will be fitted in the exit pit and will pull a drill pipe back through the bore to the entry side.
- 9. Once all bore holes have been completed, a towing assembly will be set up on the drill and this will pull the ducting into the bore.
- 10. The steel boxes will be removed, with the drilling fluid disposed of to a licensed facility.
- 11. The ducts will be cleaned and proven and their installed location surveyed.
- 12. The entry and exit pits will be reinstated to the specification of ESB Networks and Clare County Council.
- 13. A transition coupler will be installed at either side of the bridge/ following the horizontal directional drilling as per ESB requirements, this will join the HDD ducts to the standard ducts.

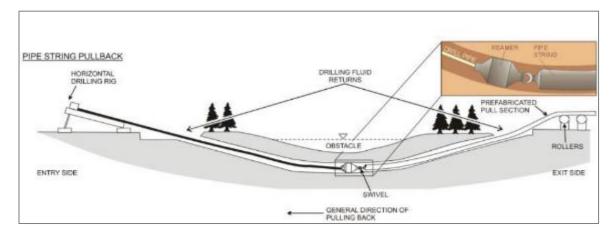


Figure 6 - Typical HDD Installation

# 7.5 Managing Excess Material from Trench

All excavated material will be temporarily stored adjacent to the trench prior to re-use in the trench reinstatement (where applicable). Stockpiles will be restricted to less than 2m in height. Where excess material exists, it may be used in the reinstatement of the Carrownagowan Wind Farm site or disposed of to a licensed facility.

# 7.6 Storage of Plant and Machinery

All plant, machinery and equipment will be stored on site within the works area or within the temporary construction compound to be located within Carrownagowan Wind Farm. Oils and fuels will not be stored on site and will be stored in an appropriately bunded area within the temporary storage compound.



## 7.7 Joint Bays and Associated Chambers

Joints Bays are to be installed approximately every 650m - 750m along the UGC route to facilitate the jointing of 2 No. lengths of UGC. Joint Bays are typically 2.5m x 6m x 1.75m pre-cast concrete structures installed below finished ground level. Joint Bays will be located in the non-wheel bearing strip of roadways, however given the narrow profile of local roads this may not always be possible.

In association with Joint Bays, Communication Chambers are required at every joint bay location to facilitate communication links between the Carrownagowan Wind Farm substation and the existing 110kV substation at Ardnacrusha. Earth Sheath Link Chambers are also required at every joint bay along the cable route. Earth Sheath Links are used for earthing and bonding cable sheaths of underground power cables, so that the circulating currents and induced voltages are eliminated or reduced. Earth Sheath Link Chambers and Communication Chambers are located in close proximity to Joint Bays. Earth Sheath Link Chambers and Communication Chambers will typically be pre-cast concrete structures with an access cover at finished surface level.

The precise siting of all Joint Bays, Earth Sheath Link Chambers and Communication Chambers is subject to approval by ESBN. Marker posts will be used on non-roadway routes to delineate the duct route and joint bay positions.

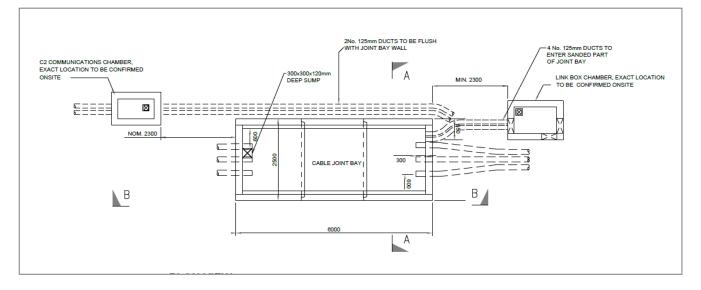


Figure 7 - 110kV Joint Bay Plan Layout

#### 7.8 Joint Bay Construction and Cable Installation

Before starting to construct, the area around the edge of the proposed joint bay which will be used by heavy vehicles will be surfaced with a terram cover if required and stone aggregate to minimise ground damage. Any roadside drains within the temporary works area will be culverted and check dams made from stone or sandbags covered with terram will be inserted upstream and downstream of these culverts to intercept any solids generated during the insertion or which wash out during the works. If the ground slopes from the working area toward a watercourse or if there is evidence of solids washing off the works area toward nearby watercourses or drains, a silt fence with straw bales, will be interposed between the works area and the watercourse.

All excavated material will be stored near the excavations and reused for reinstatement works. Any soil required for reinstatement that will be temporarily stockpiled on site will be placed at least 15m back from the nearest watercourse on level ground and will be ringed at the base by silt fencing and be regularly monitored by a



designated competent person for signs of solids escape. In which case an additional line of silt fencing with straw bales will be added in line with the relevant ECM.

If the joint bay needs to be dewatered, this will be pumped to a percolation area if the soil is not saturated, otherwise a settlement tank will be used to remove any solids from the dewatering process to comply with the ECM.

The risk of concrete reaching surface waters is considered very low given that all concrete will be poured into the pit excavated for the joint bay so that spills will be contained. The basic requirement therefore is that all pouring operations be constantly supervised to prevent accidental spillages occurring outside the pit.

Temporary storage of cement bound sand (if required) will be on hardstand areas only where there is no direct drainage to surface waters and where the area has been bunded e.g. using sand-bags and geotextile sheeting or silt fencing to contain any solids in run-off.

The following steps outline the methodology for joint bay construction and reinstatement:

- 1. The contractor will excavate a pit for joint bay construction, including for a sump in one corner.
- 2. Grade and smooth floor; then lay a 75 mm depth of blinding concrete (for in situ construction) or 50 mm thick sand (for pre-cast concrete construction) on 200 mm thick Clause 804 granular material.
- 3. In situ construction. Construct 200 mm thick reinforced concrete floor slab with sump and starter bars placed for walls as detailed on the drawings.
- In situ construction. Construct 200 mm thick reinforced concrete sidewalls as detailed on the drawings. (Figure 7)



Figure 8 - Typical joint bay under construction (in-situ)

 In situ construction. Remove formwork and backfill with suitable backfill material in grassed areas or Clause 804 material once ducting has been placed in the bay. Backfill externally with granular material to Co. Council/TII Specification for Roadworks. (Figure 8)





Figure 9 - Completed joint bay prior to cable installation (in-situ)

6. Pre-cast concrete construction. Place pre-cast concrete sections on sand bedding. (Figure 9)



Figure 10 - Typical joint bay under construction (pre-cast)

- 7. Where joint bays are located under the road surface the joint bay will be backfilled with compacted layers of Clause 804 and the road surface temporarily reinstated as specified by the local authority.
- 8. Precast concrete covers may be used as temporary reinstatement of joint bays at off road locations. These covers are placed over the constructed joint bay and are then removed at the cable installation stage of the project.
- 9. At a later date to facilitate cable installation and jointing, reinstate traffic management signage, secure individual sites, re-excavate three consecutive joint bays and store excavated material for reuse.
- 10. The cable is supplied in pre-ordered lengths on large cable drums (**Figure 10**). Installing "one section" of cable normally involves pulling three individual conductors into three separate ducts. The cable pulling winch must be set at a predetermined cut off pulling tension as specified by the designer. The cable will be connected to the winch rope using approved suitably sized and rated cable pulling stocking and swivel or the pulling head fitted by the cable manufacturer. A sponge may also be secured to the winch rope to disperse lubricant through the duct. Lubrication is also applied to the cable in the joint bay before it enters the duct.





Figure 11 - HV cable pulling procedure (Typical drum set-up)

Once the "two sections" of cable (total of 6 conductors) are pulled into the joint bay, a jointing container is positioned over the joint bay and the cable jointing procedure is carried out in this controlled environment. (Figure 12)



Figure 12 - HV cable jointing container

12. Following the completion of jointing and duct sealing works in the joint bay, place and thoroughly compact cement-bound sand in approximately 200 mm layers to the level of the cable joint base to provide vertical support. Install additional layers of cement-bound sand and compact each layer until the cement-bound sand is level with the top of the joint. Install an additional 100 mm cement-bound sand layer. Install cable protection strip. Backfill with cement-bound sand to a depth of 250 mm below surface and carry out permanent reinstatement including placement of warning tape at 400 mm depth below finished surface.

# Equipment:

- 2-3 General Operatives
- 1 Excavator Operator
- 360° tracked excavator (13 ton normally, 22 ton for rock breaker)
- 1 no. tracked dumper or tractor and trailer



# Materials:

- Sand for pipe bedding
- Blinding Concrete where necessary
- Clause 804 Material
- 160mm diameter HDPE ducting;
- 125mm diameter HDPE ducting;
- Precast Chamber Units / Relevant construction materials for chambers
- Link Box

# 8.0 Relocation of Existing Services

In order to facilitate the installation of the proposed underground cable, it may be necessary to relocate existing underground services such as water mains, gas networks or existing cables. In advance of any construction activity, the contractor will undertake detailed surveys and scans of the proposed route to confirm the presence or otherwise of any services. If found to be present, the relevant service provider will be consulted with in order to determine the requirement for specific excavation or relocation methods and to schedule a suitable time to carry out works.

# 9.0 Major Watercourse Crossings

The proposed cable route will involve 9 No. bridge crossings including 7 No. HDD crossings and 2 No. crossings in the road on the bridge. Where the cable route intersects with existing watercourses, a detailed construction method statement will be prepared by the Contractor prior to the commencement of construction and is to be approved by the Local Authority and relevant environmental agencies. The cable will be located within the bridge deck where there is sufficient depth and width available on the bridge, where there is insufficient depth and width available on the bridge, where there is insufficient depth and width available on an alternative.

Inland Fisheries Ireland have published guidelines relating to construction works along water bodies entitled 'Requirements for the Protection of Fisheries Habitats during Construction and Development Works at River Sites", and these guidelines will be adhered to during the construction of the proposed development.

Numerous other minor watercourses crossing locations have been noted along the proposed cable route i.e. culverts, pipe drains. The majority of these minor watercourses have been identified as part of the survey works and a proposed crossing schedule has been included as part of this report, see Appendix A.



## 9.1 Bridge 1 - Horizontal Directional Drilling

#### Coordinates: 52.740281, -8.616893

Bridge 1 has insufficient room to install the cable to ESB specification (450mm cover to top of ducts) and the suitability of the bridge is inadequate to accommodate the proposed works. It is proposed to horizontal directional drill (HDD) approximately 1500mm beneath the waterway and bridge foundations. This depth is based on locating a suitable clay/silt formation for HDD and the required depth may increase subject to geotechnical investigations. Drilling will take place from the road carriageway.

See Drawing 05641-231 for further details.



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Figure 14 - Bridge 1

Figure 13 - Bridge 1 Location

#### 9.2 Bridge 2 - Horizontal Directional Drilling

#### Coordinates: 52.743186, -8.60830

Bridge 2 has insufficient room to install the cable to ESB specification (450mm cover to top of ducts) and the suitability of the bridge is inadequate to accommodate the proposed works. It is proposed to horizontal directional drill (HDD) approximately 1500mm beneath the waterway and bridge foundations. This depth is based on locating a suitable clay/silt formation for HDD and the required depth may increase subject to geotechnical investigations. Drilling will take place from the road carriageway.

See Drawing 05641-232 for further details.





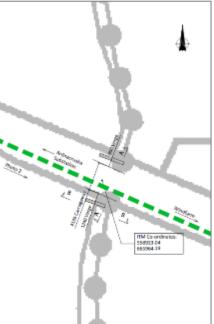


Figure 15 Bridge 2

Figure 16 Bridge 2 Location

# 9.3 Bridge 3 - Horizontal Directional Drilling

# Coordinates: 52.742639, -8.592507

Bridge 3 has insufficient room to install the cable to ESB specification (450mm cover to top of ducts) and the suitability of the bridge is inadequate to accommodate the proposed works. It is proposed to horizontal directional drill (HDD) approximately 1500mm beneath the waterway and bridge foundations. This depth is based on locating a suitable clay/silt formation for HDD and the required depth may increase subject to geotechnical investigations. Drilling will take place from the road carriageway.

See Drawing 05641-233 for further details.



Figure 17 Bridge 3

Figure 18 Bridge 3 Location



## 9.4 Bridge 4 – Instatement within Road deck

#### Coordinates: 52.786869, -8.558068

Bridge 4 has been found to have sufficient deck cover within the structure to accommodate UGC to comply with specifications. The installation can be carried out within a Trefoil arrangement with a depth of 1315mm. This permanent reinstatement of a local route can be seen as per Drawing No. 05441-222 with reinstatement of the bridge deck to be carried and will be completed to the specification of the Local Authority.

See Drawing 05641-234 for further details.



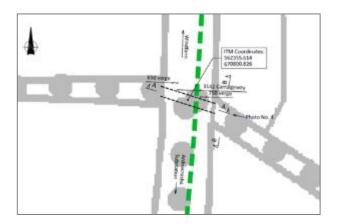


Figure 19 Bridge 4

Figure 20 Bridge 4 Location

#### 9.5 Bridge 5 - Horizontal Directional Drilling

#### Coordinates: 52.796315, -8.557663

Bridge 5 has insufficient room to install the cable to ESB specification (450mm cover to top of ducts) and the suitability of the bridge is inadequate to accommodate the proposed works. It is proposed to horizontal directional drill (HDD) approximately 1500mm beneath the waterway and bridge foundations. This depth is based on locating a suitable clay/silt formation for HDD and the required depth may increase subject to geotechnical investigations. Drilling will take place from the road carriageway.

See Drawing 05641-235 for further details.





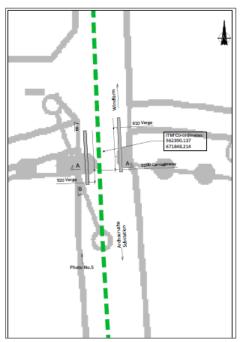


Figure 21 - Bridge 5

Figure 22 - Bridge 5 Location

# 9.6 Bridge 6 - Horizontal Directional Drilling

#### Coordinates: 52.803452, -8.563740

Bridge 6 has insufficient room to install the cable to ESB specification (450mm cover to top of ducts) and the suitability of the bridge is inadequate to accommodate the proposed works. It is proposed to horizontal directional drill (HDD) approximately 1500mm beneath the waterway and bridge foundations. This depth is based on locating a suitable clay/silt formation for HDD and the required depth may increase subject to geotechnical investigations. Drilling will take place from the road carriageway.

See Drawing 05641-236 for further details.



Figure 24 Bridge 6



Figure 23 Bridge 6 location



#### 9.7 Bridge 7 – Raise Road Level

#### Coordinates: 52.805521, -8.569268

It is proposed to cross Bridge 7 by installing the cable ducts in a trench on the deck of the bridge. Initial visual surveys have indicated insufficient room to install the cable to ESB specification (450mm cover to ducts) as per the current bridge design. The road finish will therefore need to be raised over the length of the bridge in order to achieve the required cover for the ducts. The height of the bridge parapets will also need to be raised in order to achieve 1250mm high guarding with the need road height. Reinstatement of works will be completed to the specification of the Local Authority.

A surface cable marker (metallic plate; 300mm x150mm to ESB standard) will be placed on the bridge where cable depth is unavoidably shallow.

Further consultation with the County Council's Roads Department will be necessary to agree if a handrail is required at 1100mm in height from the highest surface on the bridge.

See Drawing 05641-237 for further details.



Figure 26 Bridge 7

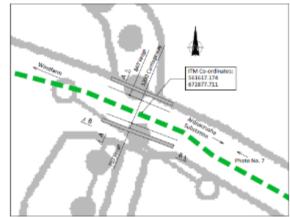


Figure 25 - Bridge 7 Location

# 9.8 Bridge 8 - Horizontal Directional Drilling

#### Coordinates: 52.806140, -8.583065

Bridge 8 has insufficient room to install the cable to ESB specification (450mm cover to top of ducts) and the suitability of the bridge is inadequate to accommodate the proposed works. It is proposed to horizontal directional drill (HDD) approximately 1500mm beneath the waterway and bridge foundations. This depth is based on locating a suitable clay/silt formation for HDD and the required depth may increase subject to geotechnical investigations. Drilling will take place from the road carriageway.



See Drawing 05641-238 for further details.



Figure 27 - Bridge 8

Figure 28 - Bridge 8 Location

# 9.9 Bridge 9 - Horizontal Directional Drilling

## Coordinates: 52.805843, -8.586053

Bridge 9 has insufficient room to install the cable to ESB specification (450mm cover to top of ducts) and the suitability of the bridge is inadequate to accommodate the proposed works. It is proposed to horizontal directional drill (HDD) approximately 1500mm beneath the waterway and bridge foundations. This depth is based on locating a suitable clay/silt formation for HDD and the required depth may increase subject to geotechnical investigations. Drilling will take place from the road carriageway.

See Drawing 05641-239 for further details.



Figure 29 - Bridge 9

Figure 30 - Bridge 9 Location



# 10.0 Reinstatement of Private Land

Once all construction works are complete, the work areas will be reinstated with excavated soil and either seeded out with native species, allowed to vegetate naturally or reinstated with excavated grass turves and will be restored to their original condition. This work will be carried out in in consultation with the landowner and in line with any relevant measures outlined in the planning application, CEMP and planning conditions.

# **11.0 Best Practice Design and Construction & Environmental Management** Methodology

Prior to commencement of construction works the contractor will draw up detailed Method Statements which will be informed by this Outline Construction Methodology, environmental protection measures included within the planning application, measures proposed within the CEMP, and the guidance documents and best practice measures listed below. This method statement will be adhered to by the contractors and will be overseen by the Project Manager, Environmental Manager and ECoW where relevant.

The following documents will contribute to the preparation of the method statements in addition to those measures proposed below: -

- Inland Fisheries Ireland (2016) *Guidelines on Protection of Fisheries during Construction Works in and Adjacent to Waters*. Inland Fisheries Ireland, *Dublin*,
- National Roads Authority (2008) Guidelines for the Crossing of Watercourses during the Construction of National Road Schemes. National Roads Authority, Dublin;
- E. Murnane, A. Heap and A. Swain. (2006) *Control of water pollution from linear construction projects.* Technical guidance (C648). CIRIA;
- E. Murnane et al., (2006) *Control of water pollution from linear construction projects*. Site guide (C649). CIRIA.
- Murphy, D. (2004) Requirements for the Protection of Fisheries Habitat during Construction and Development Works at River Sites. Eastern Regional Fisheries Board, Dublin;
- H. Masters-Williams et al (2001) Control of water pollution from construction sites. Guidance for consultants and contractors (C532);
- Enterprise Ireland (unknown). Best Practice Guide (BPGCS005) Oil storage guidelines;
- Law, C. and D'Aleo, S. (2016) Environmental good practice on site pocket book. (C762) 4th edition. CIRIA;
- CIRIA Environmental Good Practice on Site (fourth edition) (C741) 2015.

The proposed works will be carried out by employing accepted good work practices during construction, and environmental management measures such as those discussed below. Please note that the following measures will be supplemented by further specific environmental protection measures that will be included in method statements prepared for specific tasks during the works and will form part of the detailed CEMP.

- All materials shall be stored at the temporary compound within the Carrownagowan Wind Farm site and transported to the works zone immediately prior to construction;
- Where drains and watercourses are crossed with underground cables, the release of sediment will be prevented through the implementation of best practice construction methodologies.

# Outline Construction Methodology 110kV Grid Connection – Carrownagowan Wind Farm May 2020



- Weather conditions will be considered when planning construction activities to minimise risk of run off from site;
- Provision of 50m exclusion zones and barriers (silt fences) between any excavated material and any surface water features to prevent sediment washing into the receiving water environment;
- If dewatering is required as part of the proposed works e.g. in trenches for underground cabling or in wet areas, water must be treated prior to discharge;
- The contractor shall ensure that silt fences are regularly inspected and maintained during the construction phase;
- If very wet ground must be accessed during the construction process bog mats/aluminium panel tracks will be used to enable access to these areas by machinery. However, works will be scheduled to minimise access requirements during winter months;
- The contractor shall ensure that all personnel working on site are trained in pollution incident control response. A regular review of weather forecasts of heavy rainfall is required, with the Contractor required to prepare a contingency plan for before and after such events;
- The contractor will carry out visual examinations of local watercourses from the proposed works during the construction phase to ensure that sediment is not above baseline conditions. In the unlikely event of water quality concerns, the Environmental Manager and ECoW will be consulted;
- Excavations will be left open for minimal periods to avoid acting as a conduit for surface water flows.
- Only emergency breakdown maintenance will be carried out on site. Emergency procedures and spillage kits will be available and construction staff will be familiar with emergency procedures.
- Appropriate containment facilities will be provided to ensure that any spills from vehicles are contained and removed off site. Adequate stocks of absorbent materials, such as sand or commercially available spill kits shall be available;
- Concrete or potential concrete contaminated water run-off will not be allowed to enter any
  watercourses. Any pouring of concrete (delivered to site ready mixed) will only be carried out in dry
  weather. Washout of concrete trucks shall be strictly confined to a designated and controlled wash-out
  area within the Carrownagowan Wind Farm site; remote from watercourses, drainage channels and
  other surface water features;
- Entry by plant equipment, machinery, vehicles and construction personnel into watercourses or wet drainage ditches shall not be permitted. All routes used for construction traffic shall be protected against migration of soil or waste water into watercourses;
- Cabins, containers, workshops, plant, materials storage and storage tanks shall not be located near any surface water channels and will be located beyond the 50m hydrological buffer at all times.

# **12.0 Invasive Species Best Practice Measures**

Invasive species can be introduced into a location by contaminated plant, machinery and equipment which were previously used in locations that contained invasive species. Good site organisation and hygiene management shall be maintained always on site, and best practice measures will be implemented, as follows:

- The contractor will prepare an Invasive Species Action Plan to be implemented during construction, and all personnel will be made aware of the requirements contained within;
- Plant and machinery will be inspected upon arrival and departure from site and cleaned/washed as necessary to prevent the spread of invasive aquatic / riparian species such as Japanese knotweed



*Fallopia japonica* and Himalayan Balsam *Impatiens glandulifera*. A sign off sheet will be maintained by the contractor to confirm the implementation of measures;

• Site hygiene signage will be erected in relation to the management of non-native invasive material.

# **13.0 Waste Management**

All waste arising during the construction phase will be managed and disposed of in a way that ensures the provisions of the Waste Management Act 1996 and associated amendments and regulations and the Waste Management Plan. Soil will be reinstated into trenches where possible. In the event, there is excess material with no defined purpose, it will be transported to an authorised soil recovery site.



# **Appendix A – Culvert Crossings**

9	Culvert Crossing Schedule							
Culvert No.	Dimensions (mm)	Material	Approx. Cover (mm)	Proposed Crossing Methodology	Photo			
1.	350 Ø	Concrete	900	UNDERCROSSING				
2.	300 Ø	HDPE	200	UNDERCROSSING				
3.	2x800 Ø	Concrete	1800	OVERCROSSING				
4.	600 wide x 800 deep	Stone	1000	UNDERCROSSING				
5.	800 Ø	HDPE	200	UNDERCROSSING				
6.	250 Ø	Concrete	500	UNDERCROSSING				
7.	600 Ø	Concrete	700	UNDERCROSSING				
8.	400 wide x 500 deep	Stone	900	UNDERCROSSING				
9.	600 wide x 500 deep	Stone	900	UNDERCROSSING				

	Culvert Crossing Schedule							
Culvert No.	Dimensions (mm)	Material	Approx. Cover (mm)	Proposed Crossing Methodology	Photo			
10.	600 Ø	HDPE	500	UNDERCROSSING				
11.	300 Ø	HDPE	600	UNDERCROSSING				
12.	2x750 Ø	HDPE	2000	OVERCROSSING				
15.	300 Ø 375 Ø	HDPE HDPE	600 700	UNDERCROSSING				
16.	375 Ø	HDPE	700	UNDERCROSSING				
17.	375 Ø	HDPE	650	UNDERCROSSING				
18.	375 Ø	HDPE	350	UNDERCROSSING				
19.	600 Ø	HDPE	800	UNDERCROSSING				

Culvert Crossing Schedule							
Culvert No.	Dimensions (mm)	Material	Approx. Cover (mm)	Proposed Crossing Methodology	Photo		
22.	600 Ø	Concrete	550	UNDERCROSSING			
23.	300 Ø	Concrete	600	UNDERCROSSING			
24.	250 Ø	HDPE	100	UNDERCROSSING			
25.		NEW CONCRETE ARCH CULVERT TO BE INSTALLED OVER RIVER		OVERCROSSING			
26.	450 Ø	CONCRETE	1000	UNDERCROSSING			
27.	300 Ø	CONCRETE	750	UNDERCROSSING			
28.	900 (Width per span)	Two Span Masonry	700	UNDERCROSSING			